



Short Course on Nonlinear Acoustics

22nd International Symposium on Nonlinear Acoustics

Oleg Sapozhnikov

Part II.

Nonlinear acoustics of fluids. Perturbation modes and related phenomena.

Radiation force. Specificity of nonlinear effects in the presence of shocks.

Acoustic, entropy, and vorticity modes

Equations for classical thermoviscous fluid

$$\rho \left[\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} \right] = -\nabla p + \eta \Delta \mathbf{v} + \left(\zeta + \frac{\eta}{3} \right) \nabla (\nabla \cdot \mathbf{v})$$

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

$$\rho T \left[\frac{\partial s}{\partial t} + (\mathbf{v} \cdot \nabla) s \right] = \kappa \Delta T + \frac{\eta}{2} \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \nabla \cdot \mathbf{v} \right)^2 + \zeta (\nabla \cdot \mathbf{v})^2$$

Thermodynamic relations

$$d\rho = dp/c^2 - ds \cdot \alpha_V T \rho / c_p$$

$$dT = dp \cdot \alpha_V T / (\rho c_p) + ds \cdot T / c_p$$

Fluid parameters

$$\alpha_V = -\rho^{-1} (\partial \rho / \partial T)_p$$

$$c = \sqrt{(\partial p / \partial \rho)_s} \quad c_p = T (\partial s / \partial T)_p$$

Linearization:

$$\rho = \rho_0 + \rho', \quad p = p_0 + p', \quad s = s_0 + s', \quad T = T_0 + T'$$

$$\begin{aligned}\frac{\partial \mathbf{v}}{\partial t} &= \frac{\eta}{\rho_0} \Delta \mathbf{v} + \frac{\zeta + \eta/3}{\rho_0} \nabla (\nabla \cdot \mathbf{v}) - \frac{1}{\rho_0} \nabla p' \\ \frac{\partial p'}{\partial t} &= -\rho_0 c_0^2 \nabla \cdot \mathbf{v} + \frac{c_0^2 \kappa \alpha_V^2 T_0}{\rho_0 c_p^2} \Delta p' + \frac{c_0^2 \kappa \alpha_V T_0}{c_p^2} \Delta s' \\ \frac{\partial s'}{\partial t} &= \frac{\kappa \alpha_V}{\rho_0^2 c_p} \Delta p' + \frac{\kappa}{\rho_0 c_p} \Delta s' \\ \rho' &= \frac{1}{c_0^2} p' - \frac{\rho_0 \alpha_V T_0}{c_p} s' \\ T' &= \frac{\alpha_V T_0}{\rho_0 c_p} p' + \frac{T_0}{c_p} s'\end{aligned}$$

The Helmholtz decomposition

Velocity is the sum of an irrotational (curl-free) and a solenoidal (divergence-free) vector fields:

$$\mathbf{v} = \nabla \varphi + \nabla \times \mathbf{A}$$

Vorticity mode:

$$\mathbf{v}_{vor} = \nabla \times \mathbf{A}$$

VORTICITY MODE

$$\frac{\partial \mathbf{v}_{vor}}{\partial t} = \frac{\eta}{\rho_0} \Delta \mathbf{v}_{vor}$$

$$\nabla \cdot \mathbf{v}_{vor} = 0$$

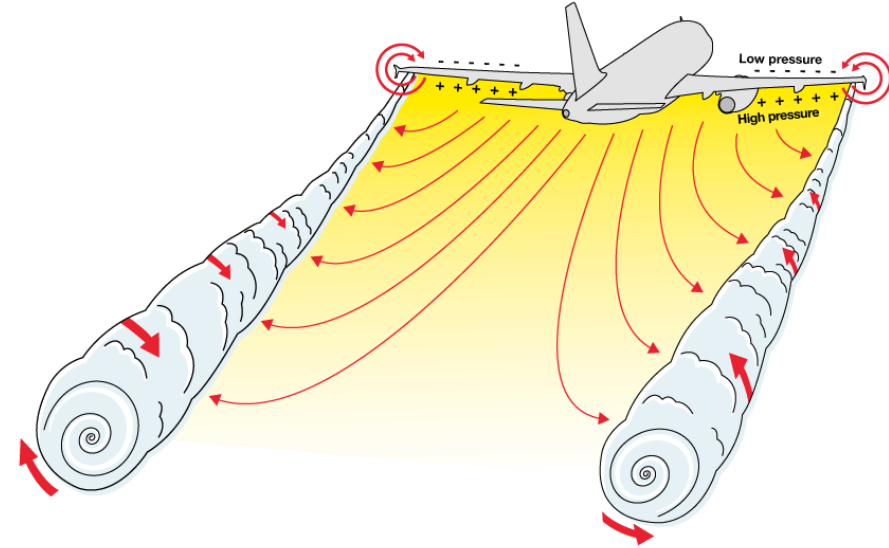
$$s_{vor} = 0$$

$$p_{vor} = 0$$

$$\rho_{vor} = 0$$

$$T_{vor} = 0$$

All aircraft generate wake vortices, also known as wake turbulence



Wake caused by a boat



POTENTIAL MOTION

$$\frac{\partial \varphi}{\partial t} = \frac{\varsigma + 4\eta/3}{\rho_0} \Delta \varphi - \frac{1}{\rho_0} p'$$

$$\frac{\partial p'}{\partial t} = -\rho_0 c_0^2 \Delta \varphi + \frac{c_0^2 \kappa \alpha_V^2 T_0}{\rho_0 c_p^2} \Delta p' + \frac{c_0^2 \kappa \alpha_V T_0}{c_p^2} \Delta s'$$

$$\frac{\partial s'}{\partial t} = \frac{\kappa \alpha_V}{\rho_0^2 c_p} \Delta p' + \frac{\kappa}{\rho_0 c_p} \Delta s'$$

$$\rho' = \frac{1}{c_0^2} p' - \frac{\rho_0 \alpha_V T_0}{c_p} s'$$

$$T' = \frac{\alpha_V T_0}{\rho_0 c_p} p' + \frac{T_0}{c_p} s'$$

ROTATIONAL MOTION

Vorticity mode

Entropy mode

Acoustic mode

ENTROPY MODE (heat diffusion)

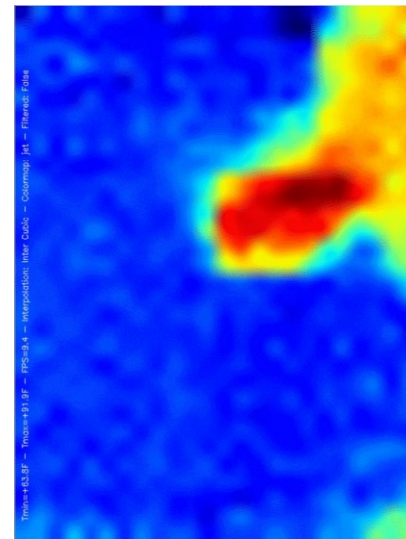
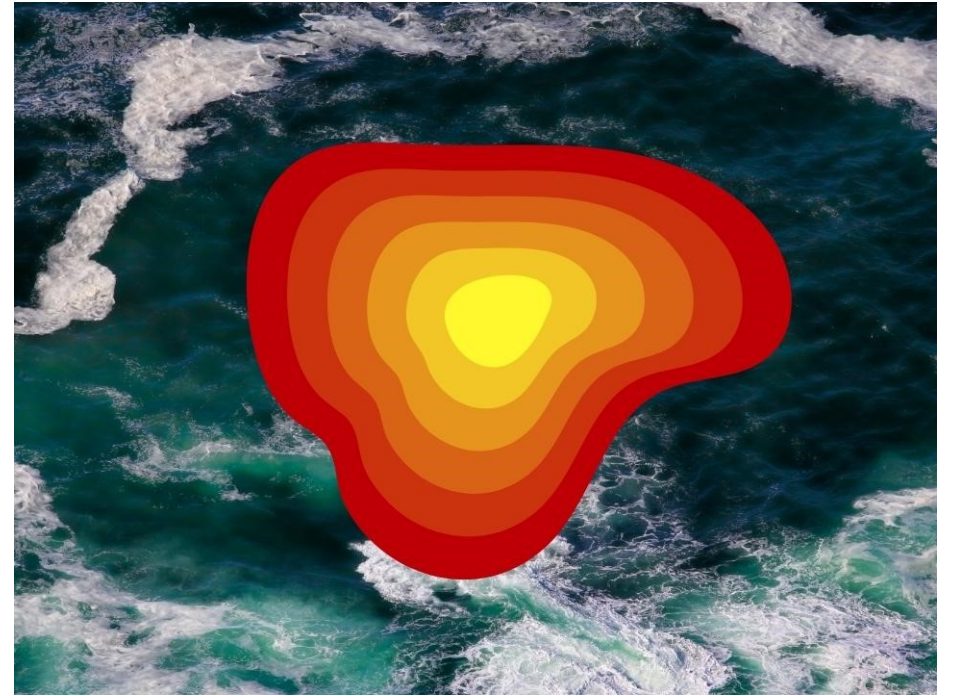
$$\frac{\partial s_{ent}}{\partial t} \approx \frac{\kappa}{\rho_0 c_p} \Delta s_{ent}$$

$$T_{ent} = T_0 / c_p \cdot s_{ent}$$

$$\rho_{ent} = -\alpha_V T_0 \rho_0 / c_p \cdot s_{ent} = -\rho_0 \alpha_V T_{ent}$$

$$p_{ent} \approx 0$$

$$\mathbf{v}_{ent} \approx \kappa \alpha_V T_0 / (\rho_0 c_p^2) \cdot \nabla s_{ent}$$



ACOUSTIC MODE (sound waves)

$$\frac{\partial^2 p_{ac}}{\partial t^2} - c_0^2 \Delta p_{ac} \approx \delta \frac{\partial}{\partial t} \Delta p_{ac}$$

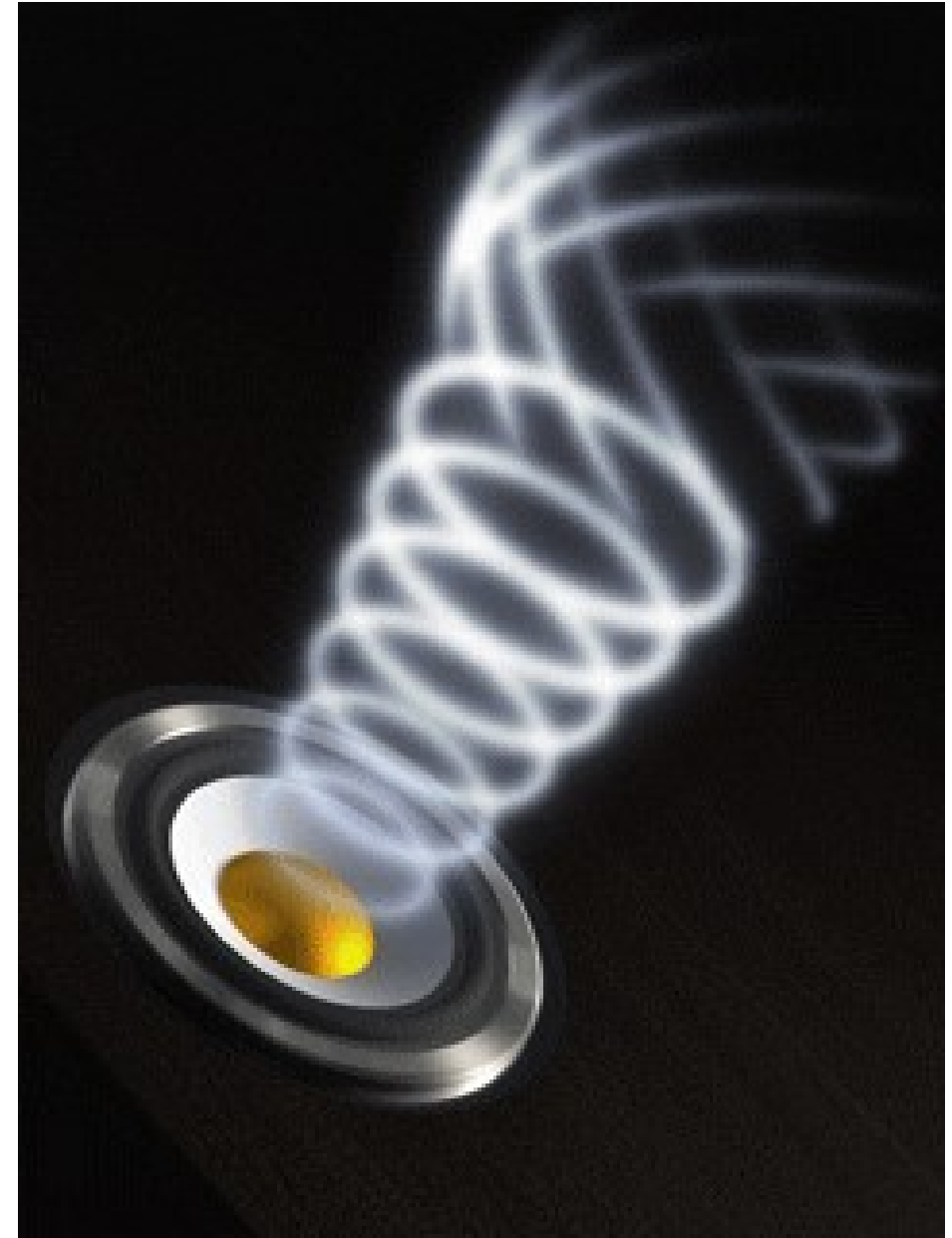
$$\frac{\partial \mathbf{v}_{ac}}{\partial t} = - \left(\frac{1}{\rho} + \frac{\zeta + 4\eta/3}{\rho^2 c^2} \frac{\partial}{\partial t} \right) \nabla p_{ac} \approx - \frac{1}{\rho} \nabla p_{ac}$$

$$\rho_{ac} = c_0^{-2} p_{ac} + c_0^{-2} \kappa (c_v^{-1} - c_p^{-1}) \nabla \cdot \mathbf{v}_{ac}$$

$$T_{ac} = \alpha_V T_0 / (\rho_0 c_p) \cdot (p_{ac} - \kappa c_p^{-1} \nabla \cdot \mathbf{v}_{ac})$$

$$s_{ac} \approx -\alpha_V \kappa / (\rho_0 c_p) \nabla \cdot \mathbf{v}_{ac}$$

$$\delta = [4\eta/3 + \zeta + \kappa (c_v^{-1} - c_p^{-1})] / \rho_0$$



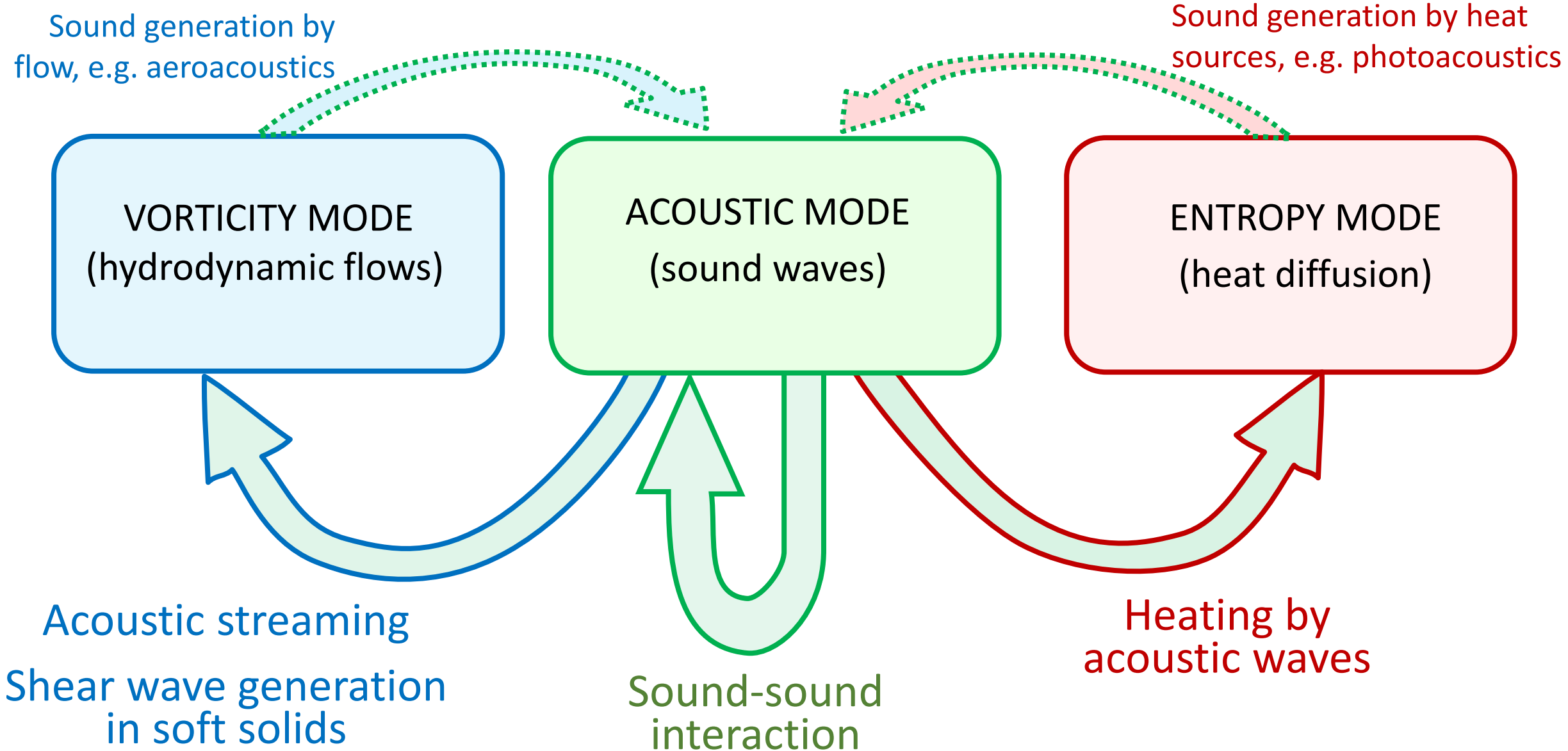
Equations for classical thermoviscous fluid

$$\rho \left[\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} \right] = -\nabla p + \eta \Delta \mathbf{v} + \left(\zeta + \frac{\eta}{3} \right) \nabla (\nabla \cdot \mathbf{v})$$

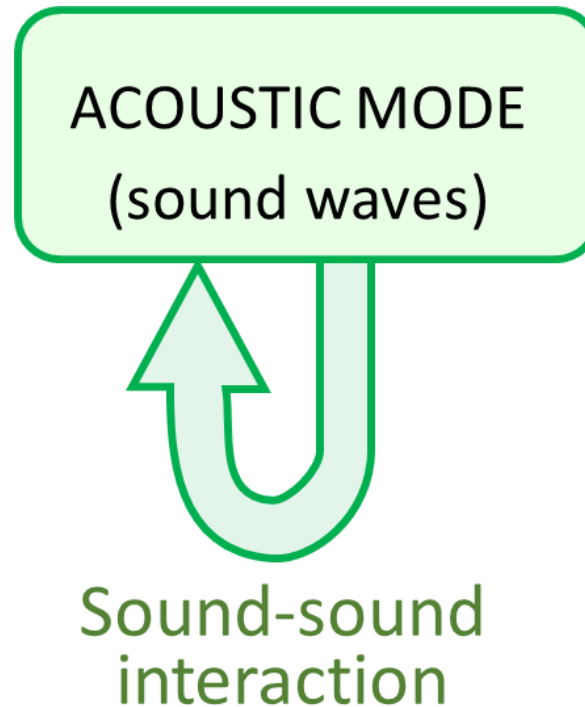
$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

$$\rho T \left[\frac{\partial s}{\partial t} + (\mathbf{v} \cdot \nabla) s \right] = \kappa \Delta T + \frac{\eta}{2} \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \nabla \cdot \mathbf{v} \right)^2 + \zeta (\nabla \cdot \mathbf{v})^2$$

THE SUBJECTS OF STUDY IN NONLINEAR ACOUSTICS

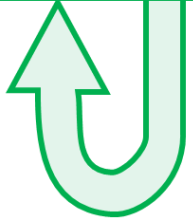


Sound-sound interaction (nonlinear phenomena within the acoustic mode)



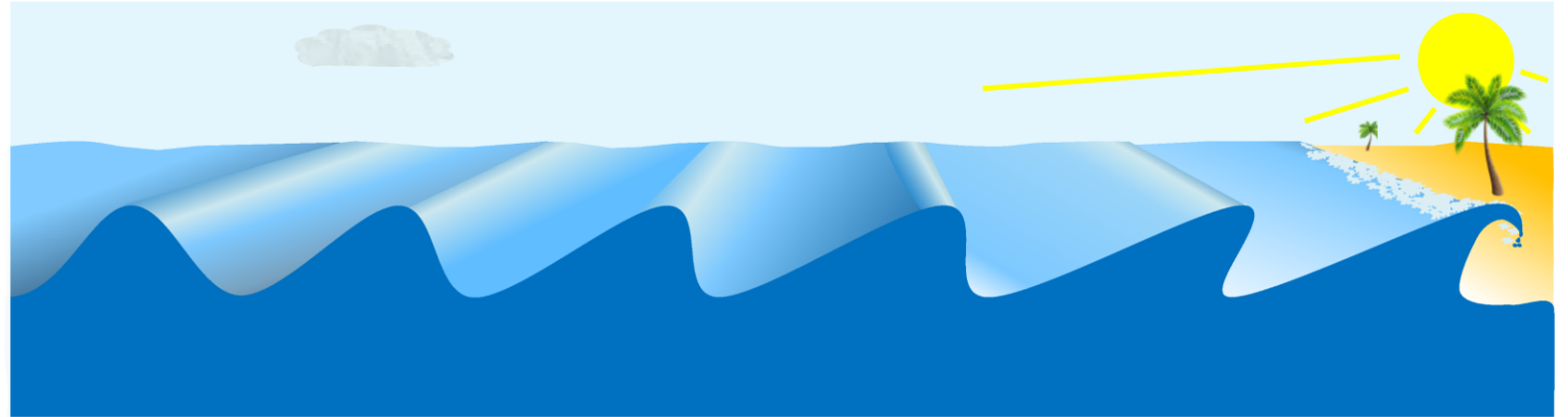
HARMONIC GENERATION

ACOUSTIC MODE
(sound waves)

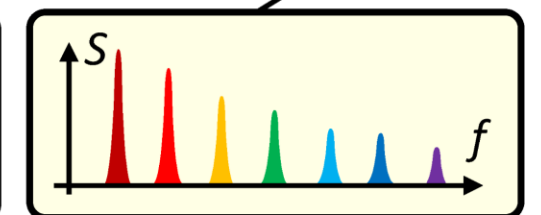
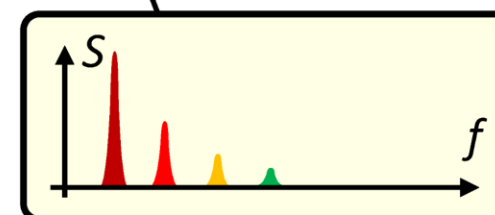
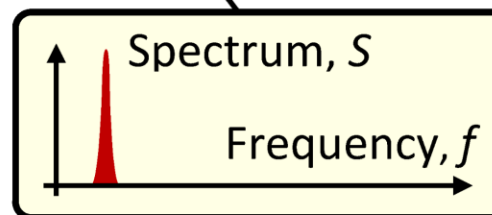
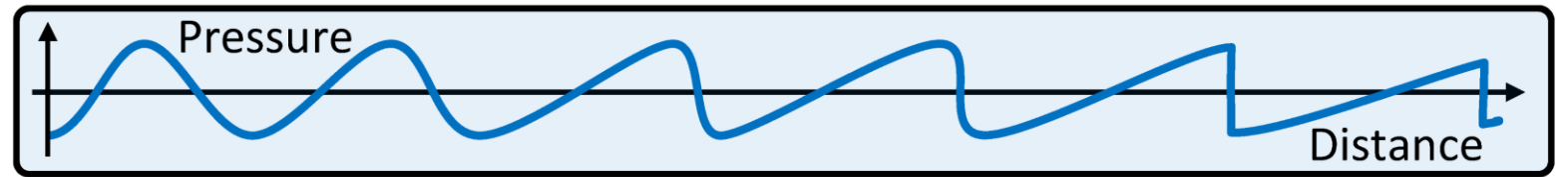


Sound-sound
interaction

WAVE ON THE SEA SURFACE



NONLINEAR ACOUSTIC WAVE



Harmonic generation as
a phonon-phonon
interaction

$$\hbar\omega + \hbar\omega = \hbar \times 2\omega$$

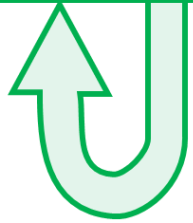
$$\hbar\omega + \hbar \times 2\omega = \hbar \times 3\omega$$

$$\omega \rightarrow 2\omega, 3\omega, \dots$$

DIFFERENCE FREQUENCY GENERATION

Parametric arrays

ACOUSTIC MODE
(sound waves)

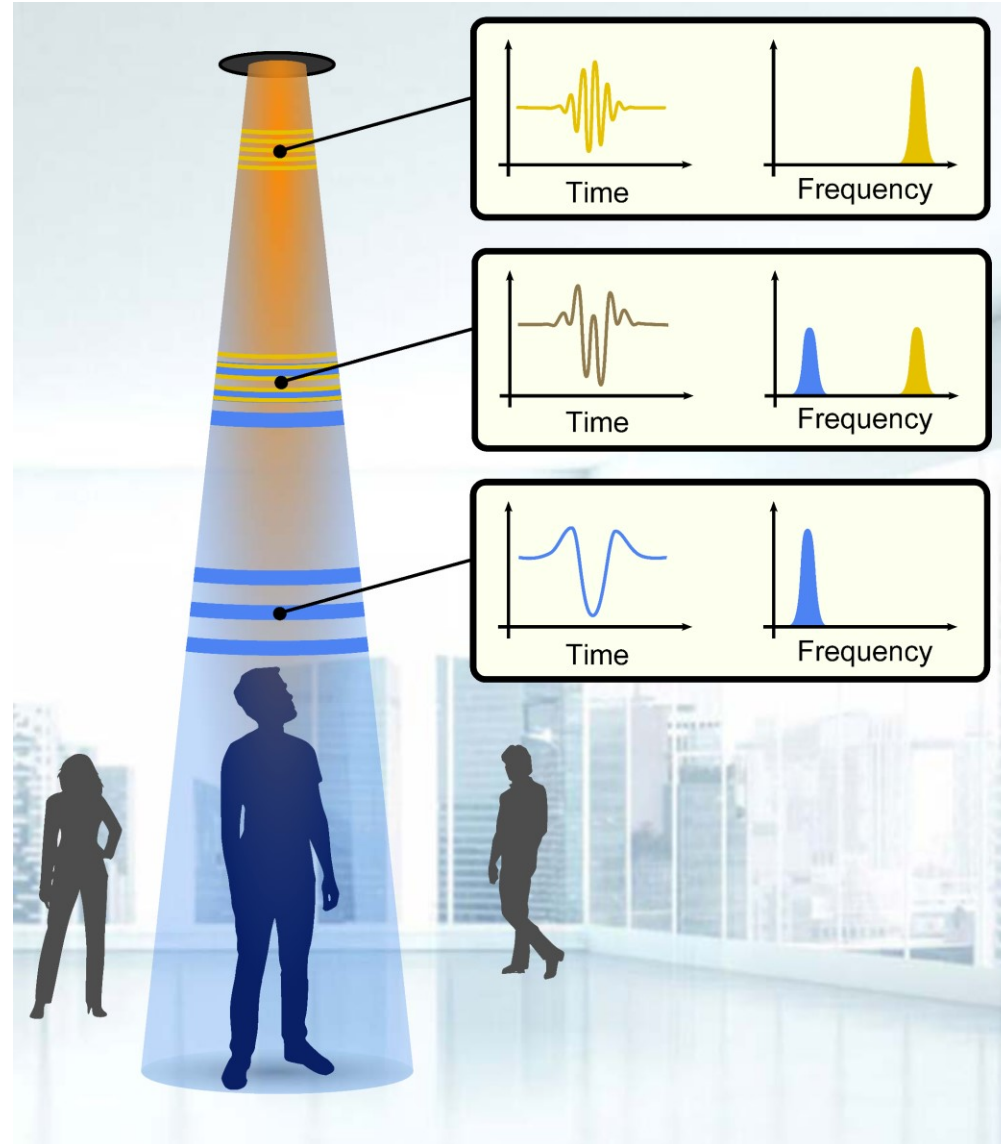


Sound-sound
interaction

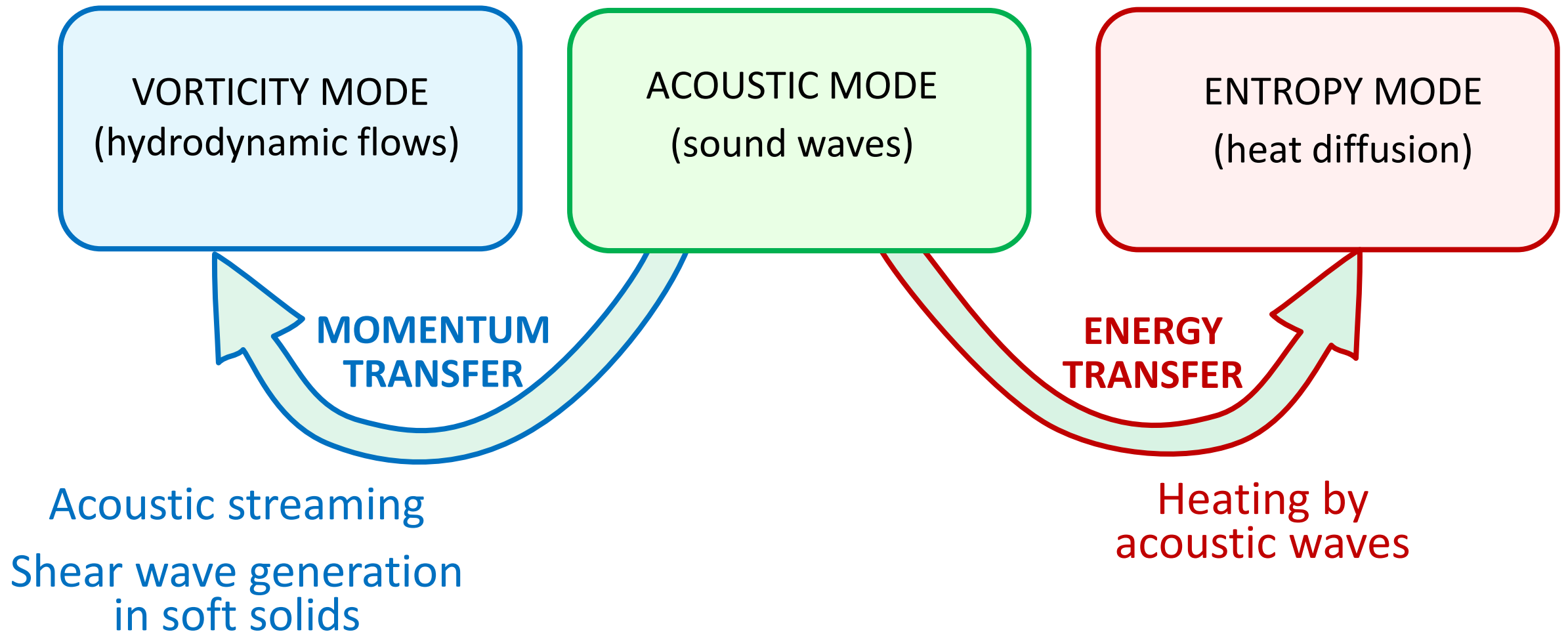
Difference frequency
generation as
a phonon-phonon interaction

$$\hbar\omega_2 - \hbar\omega_1 = \hbar \times (\omega_2 - \omega_1)$$

$$\omega_1, \omega_2 \rightarrow \Omega = \omega_2 - \omega_1$$



THE SUBJECTS OF STUDY IN NONLINEAR ACOUSTICS



MOMENTUM VS PSEUDO-MOMENTUM

The calculation of the momentum of acoustic waves requires taking into account the nonlinear terms of the second order. However, in many practical cases (lossless medium, open space) the second-order terms cancel each other out, and it is possible to define a pseudo-momentum that is expressed by only the terms of the linear approximation.

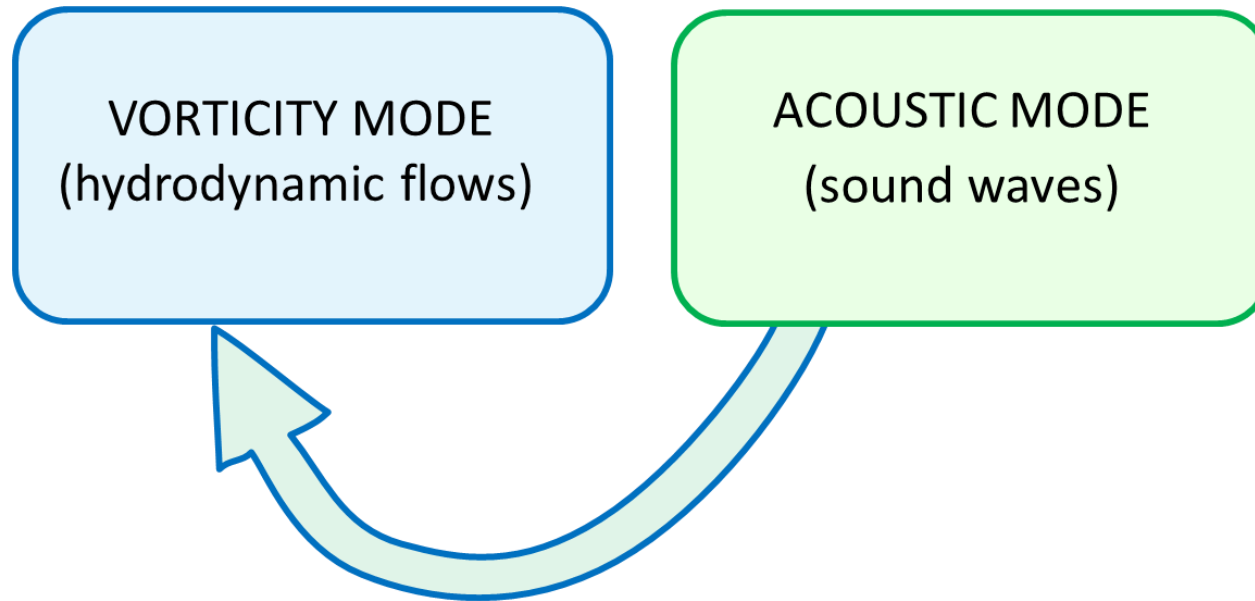
McIntyre, J. Fluid Mech. 1981 formulated 'the pseudo-momentum rule':

The mean forces on the obstacle are often same **as if**

- (a) the waves had momentum equal to their pseudo-momentum and
- (b) the medium were absent.

In the acoustic example of the radiation force on an absorber in a pipe with rigid walls, the pseudo-momentum rule is NOT satisfied – there is an average isotropic stress of the second order of smallness. However, if the tube walls are allowed to expand outward under the action of the radiation stress, this will lead to an adjustment of the mean pressure field, which can compensate for the isotropic component of the radiation stress, and the pseudo-momentum rule becomes valid.

Excitation of the vorticity mode by sound (transfer of momentum from sound to medium)



NONLINEAR ACOUSTIC PHENOMENA CAUSED BY WAVE MOMENTUM TRANSFER

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graph TD; A[NONLINEAR ACOUSTIC PHENOMENA CAUSED BY WAVE MOMENTUM TRANSFER] --> B[Acoustic streaming]; A --> C[Acoustic fountain]; A --> D[Shear wave generation in soft solids]; A --> E[Radiation force acting on absorbers]; A --> F[Radiation force acting on scatterers];
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Acoustic
streaming

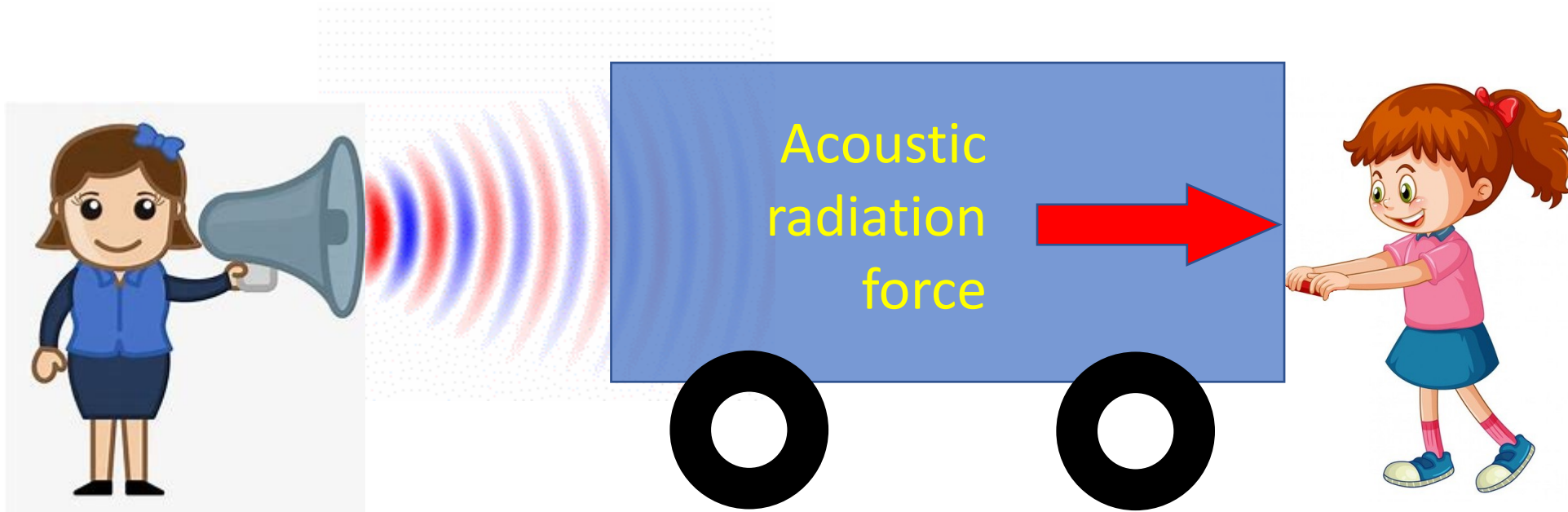
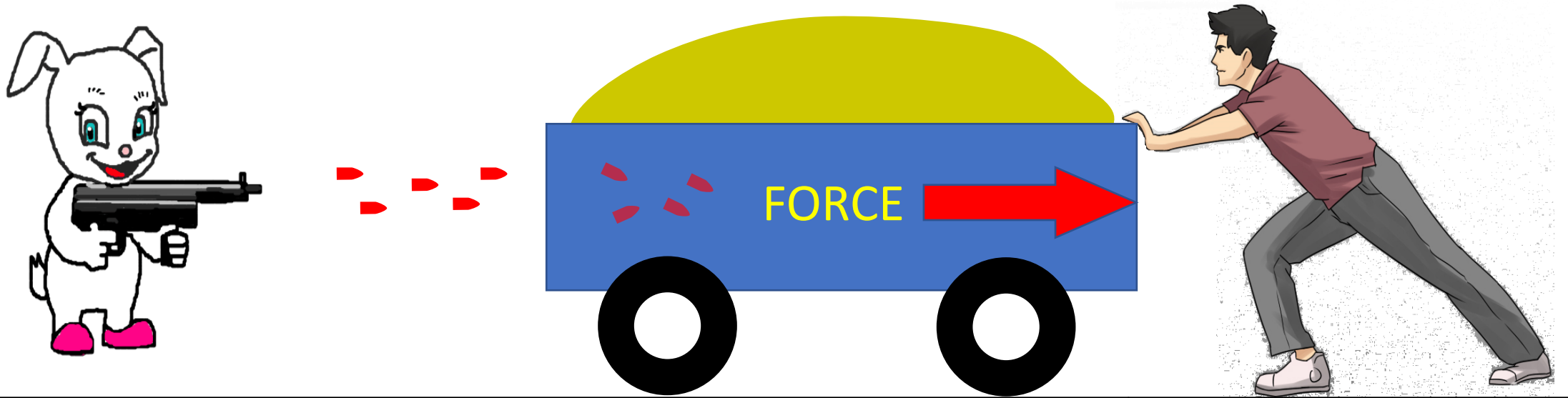
Acoustic
fountain

Shear wave
generation in soft
solids

Radiation force
acting on
absorbers

Radiation force
acting on
scatterers

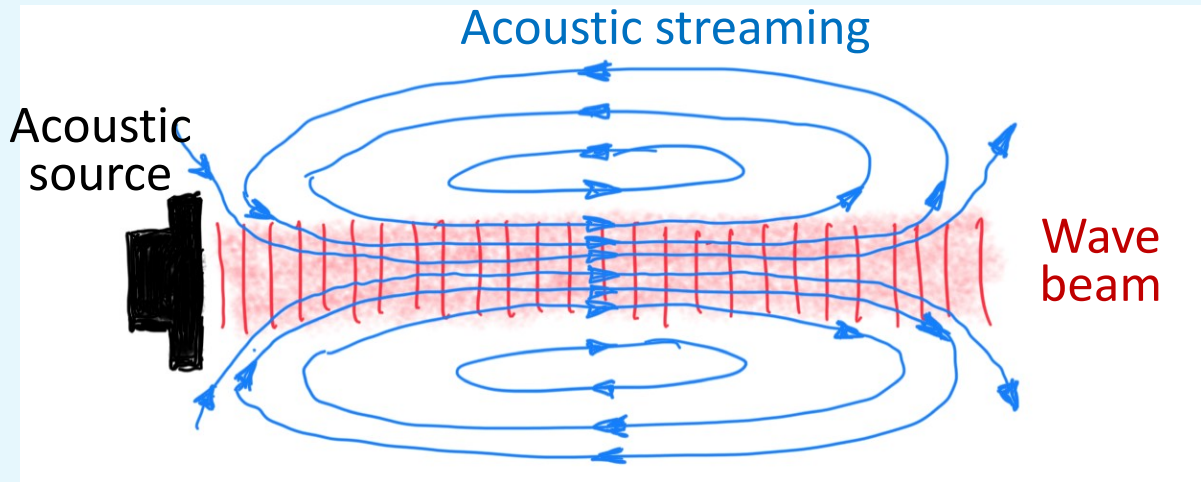
Transfer of momentum results in force



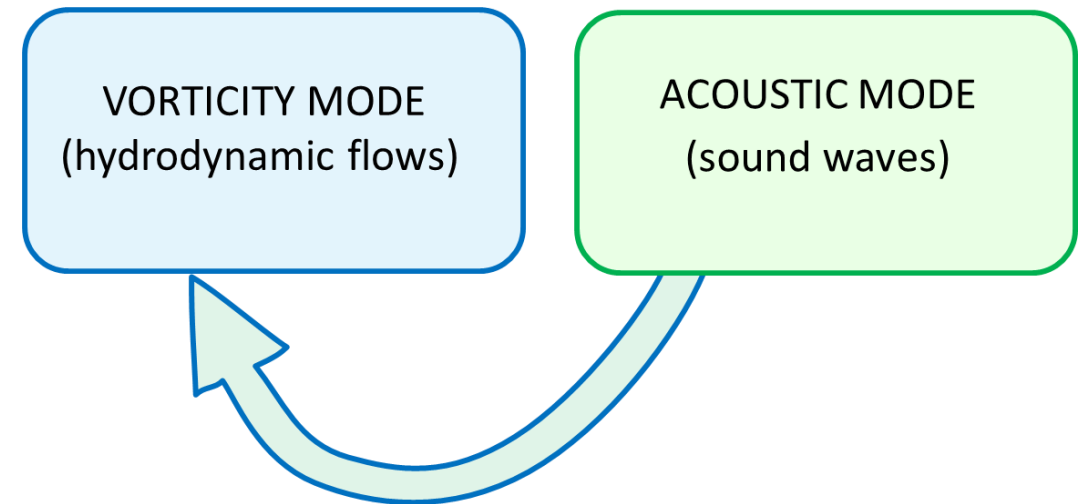
ACOUSTIC STREAMING

ECKART STREAMING

Caused by sound absorption during propagation in bulk flow



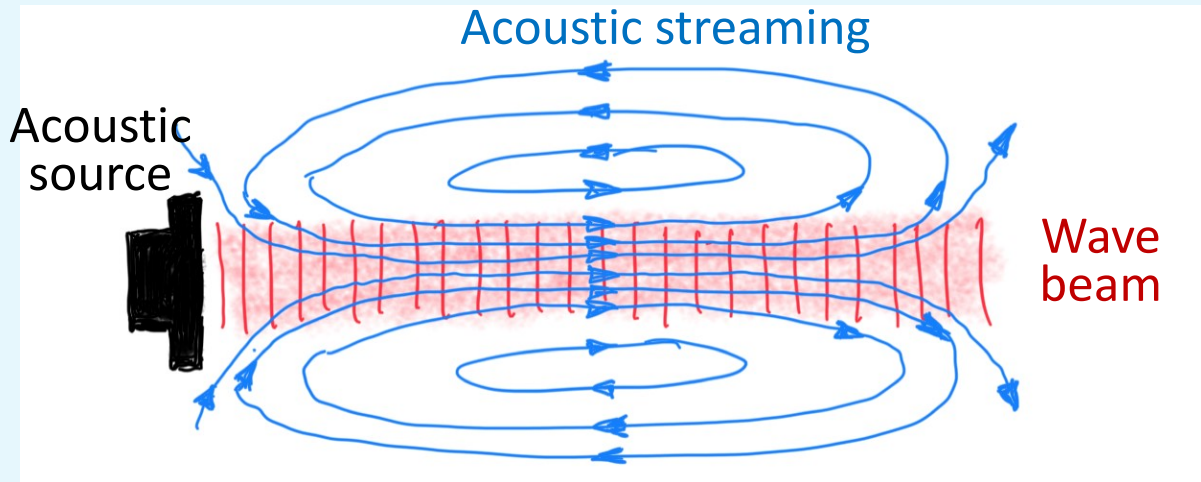
RAYLEIGH STREAMING - Caused by sound absorption near a boundary, either when sound reaches a boundary, or when a boundary is vibrating in a still medium.



ACOUSTIC STREAMING

ECKART STREAMING

Caused by sound absorption during propagation in bulk flow



RAYLEIGH STREAMING - Caused by sound absorption near a boundary, either when sound reaches a boundary, or when a boundary is vibrating in a still medium.

Governing equations:

$$\rho_0 \left[\frac{\partial \mathbf{U}}{\partial t} + (\mathbf{U} \cdot \nabla) \mathbf{U} \right] = -\nabla P + \eta \Delta \mathbf{U} + \mathbf{f} ,$$
$$\nabla \cdot \mathbf{U} = 0 ,$$

$\mathbf{U} = \langle \rho \mathbf{v} \rangle / \rho_0$ – streaming velocity,

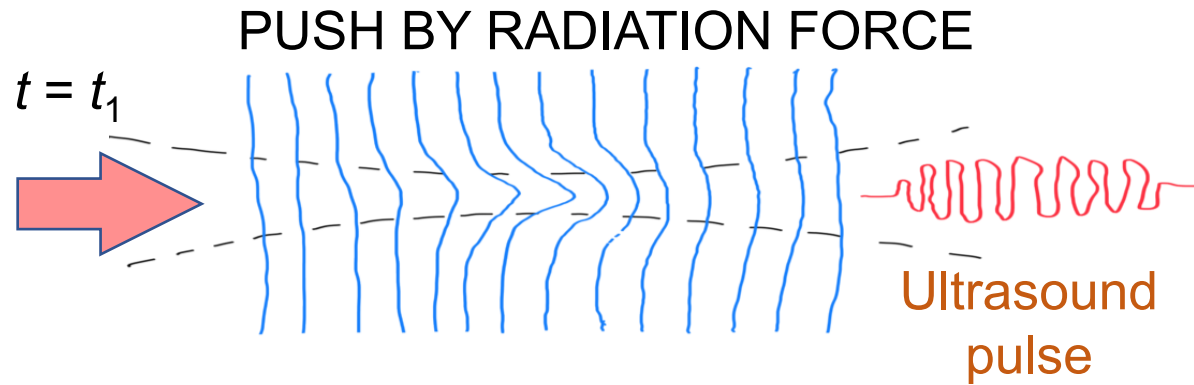
$\mathbf{f} = -\rho_0 \langle (\mathbf{v}_{ac} \cdot \nabla) \mathbf{v}_{ac} + \mathbf{v}_{ac} (\nabla \cdot \mathbf{v}_{ac}) \rangle$
– radiation force per unit mass of liquid,
 $\langle \dots \rangle$ – averaging over the wave period.

For a harmonic wave of arbitrary spatial structure:

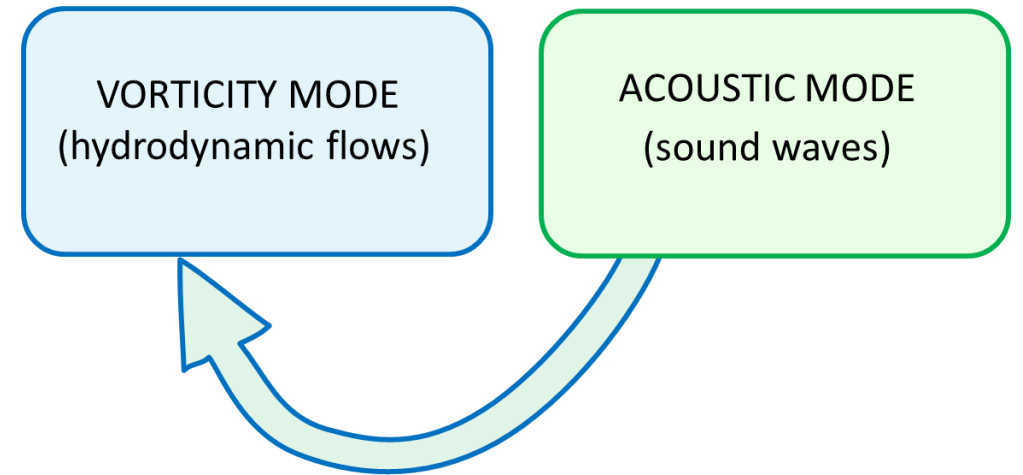
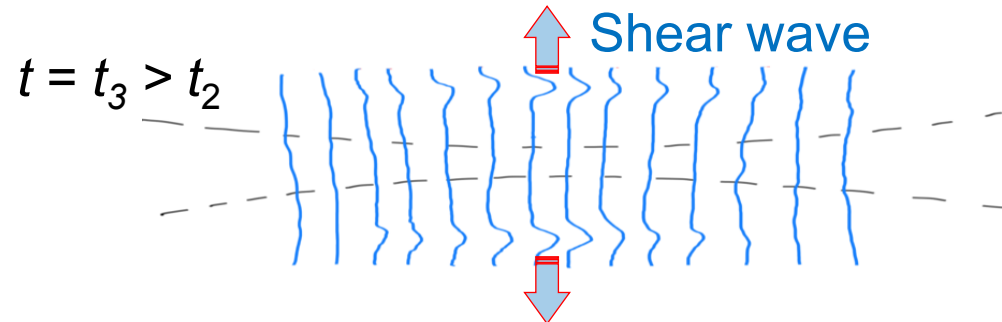
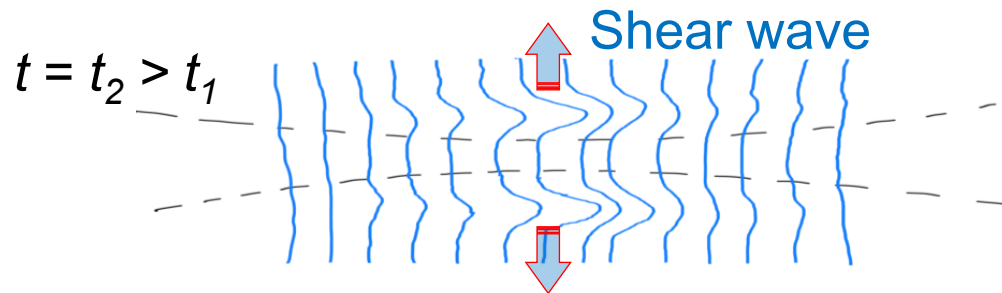
$$\mathbf{f} = \frac{2\alpha}{c_0} \mathbf{I}$$

$\mathbf{I} = \langle p_{ac} \mathbf{v}_{ac} \rangle$ – wave intensity

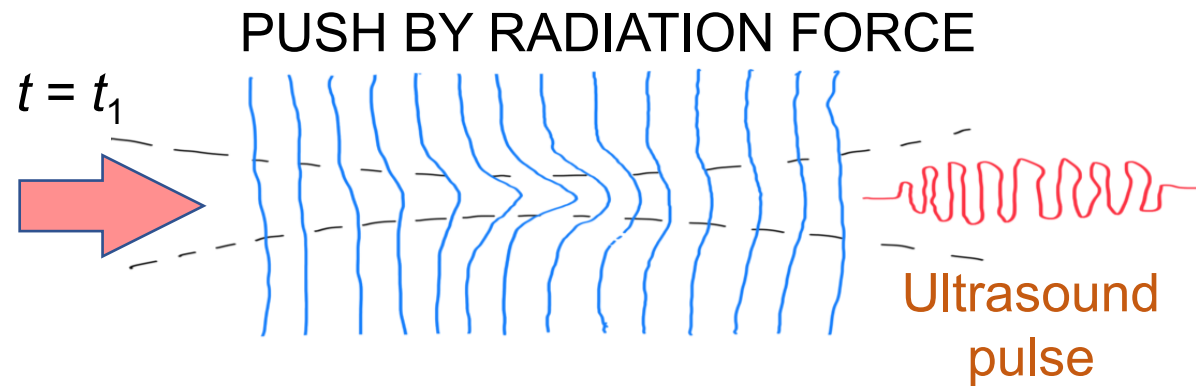
SHEAR WAVE GENERATION IN SOFT SOLIDS



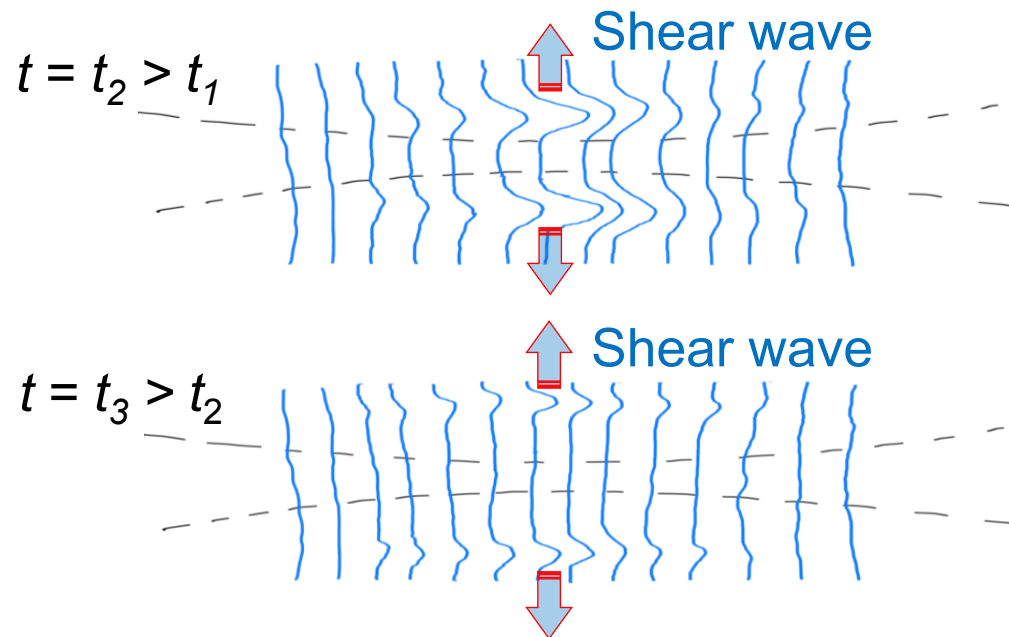
RELAXATION IN THE FORM OF
AN OUTGOING SHEAR WAVE



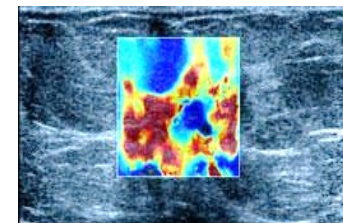
SHEAR WAVE GENERATION IN SOFT SOLIDS



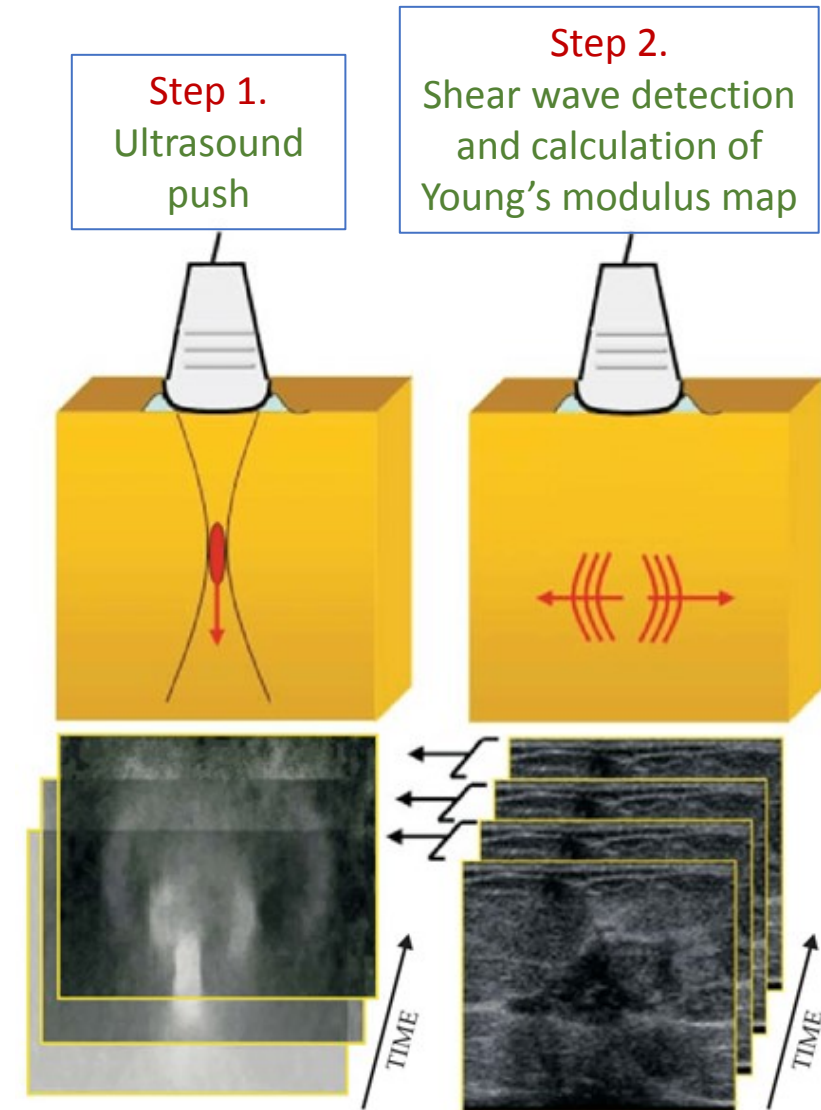
RELAXATION IN THE FORM OF AN OUTGOING SHEAR WAVE



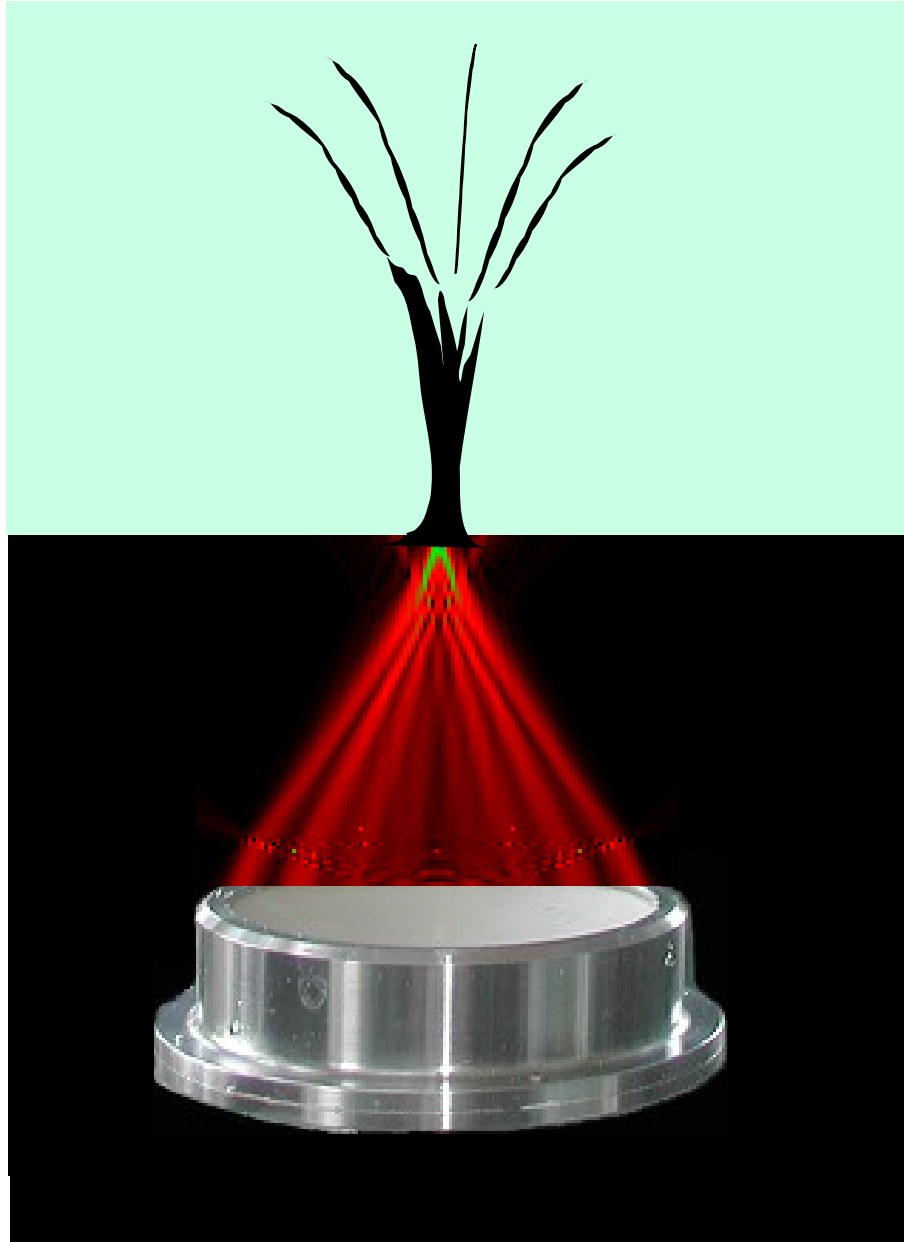
«Aixplorer»
Supersonic
Imaging



Shear wave elastography



ACOUSTIC FOUNTAIN

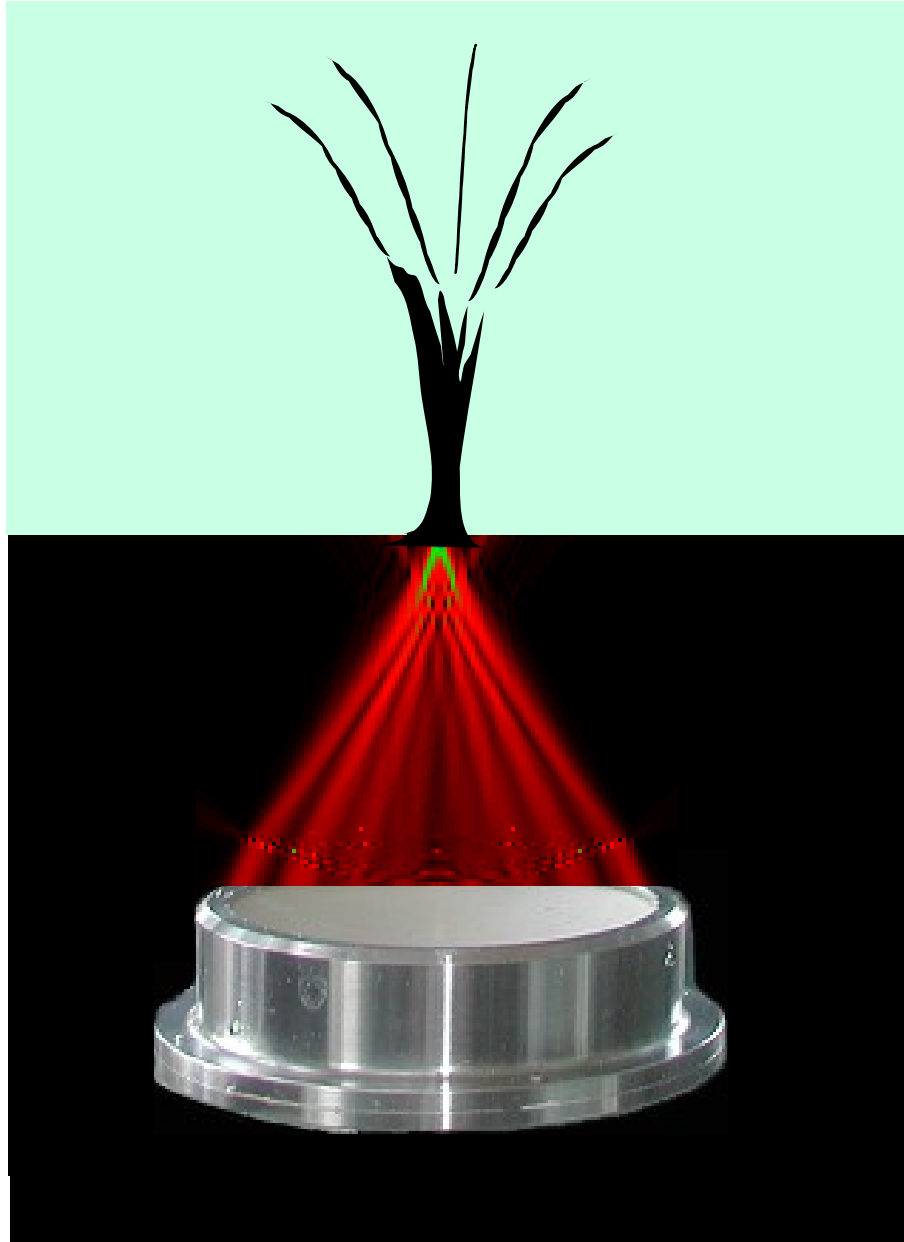


VORTICITY MODE
(hydrodynamic flows)

ACOUSTIC MODE
(sound waves)



ACOUSTIC FOUNTAIN



HIFU-induced acoustic fountain



HIFU-induced acoustic fountain and atomization



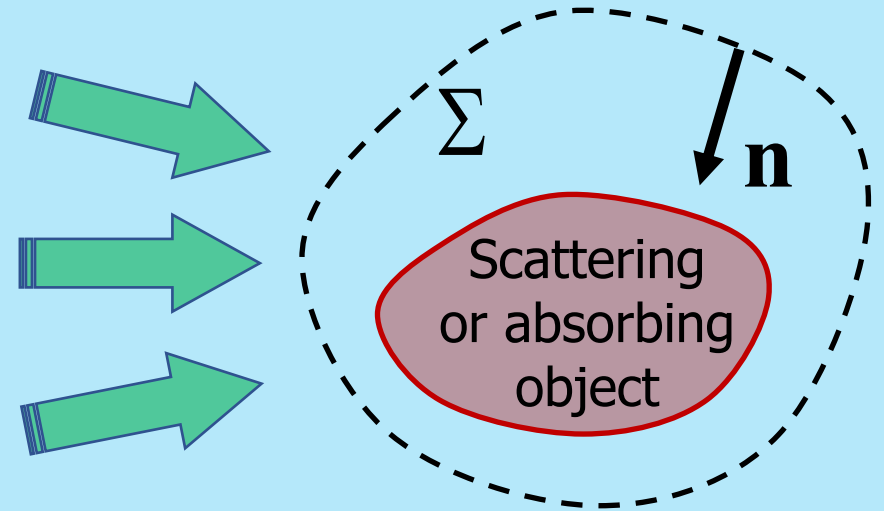
RADIATION FORCE ACTING ON ABSORBERS AND SCATTERERS

Momentum flux tensor (after Langevin):

$$T_{ij} = \left(\frac{p^2}{2\rho_0 c_0^2} - \frac{\rho_0 \mathbf{v} \cdot \mathbf{v}}{2} \right) \delta_{ij} + \rho_0 v_i v_j ,$$

$$\mathbf{v} = (v_1, v_2, v_3)$$

Radiation force:
$$F_i = - \oiint_{\Sigma} \langle T_{ij} \rangle n_j ds$$



Acoustic pressure
in CW case:

$$p' = \text{Re} \left(P \cdot e^{-i\omega t} \right)$$

Particle velocity
complex amplitude: $\mathbf{V} = \nabla P / (i\rho\omega)$

Radiation force as a functional of a CW acoustic field:

$$\mathbf{F} = \oiint_S \left\{ \left(\frac{\rho |\mathbf{V}|^2}{4} - \frac{|P|^2}{4\rho c^2} \right) \mathbf{n} - \frac{\rho}{2} \text{Re} \left[\mathbf{V}^* (\mathbf{V} \cdot \mathbf{n}) \right] \right\} dS$$

$$\mathbf{F} = \oint_S \left\{ \left(\frac{\rho |\mathbf{V}|^2}{4} - \frac{|P|^2}{4\rho c^2} \right) \mathbf{n} - \frac{\rho}{2} \text{Re}[\mathbf{V}^* (\mathbf{V} \cdot \mathbf{n})] \right\} dS$$

Plane wave case: $\mathbf{V} = -\frac{P}{\rho c} \mathbf{n}$

$$F = \iint_{\text{absorber surface}} \frac{|P|^2}{2\rho c^2} dS \Rightarrow F = \frac{W}{c}$$

W - total acoustic power

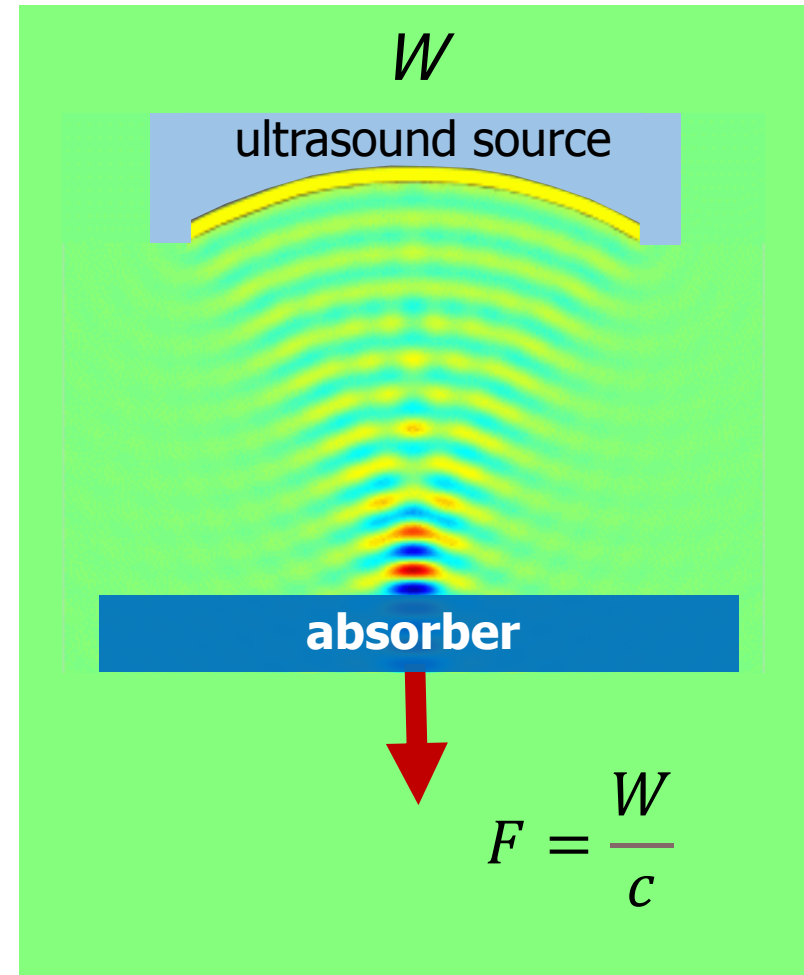
Interpretation in terms of phonon energy and momentum

Quasi-momentum: $\Delta N = \hbar k = \hbar \frac{\omega}{c} = \frac{\Delta E}{c}$

Energy: $\Delta E = \hbar \omega$

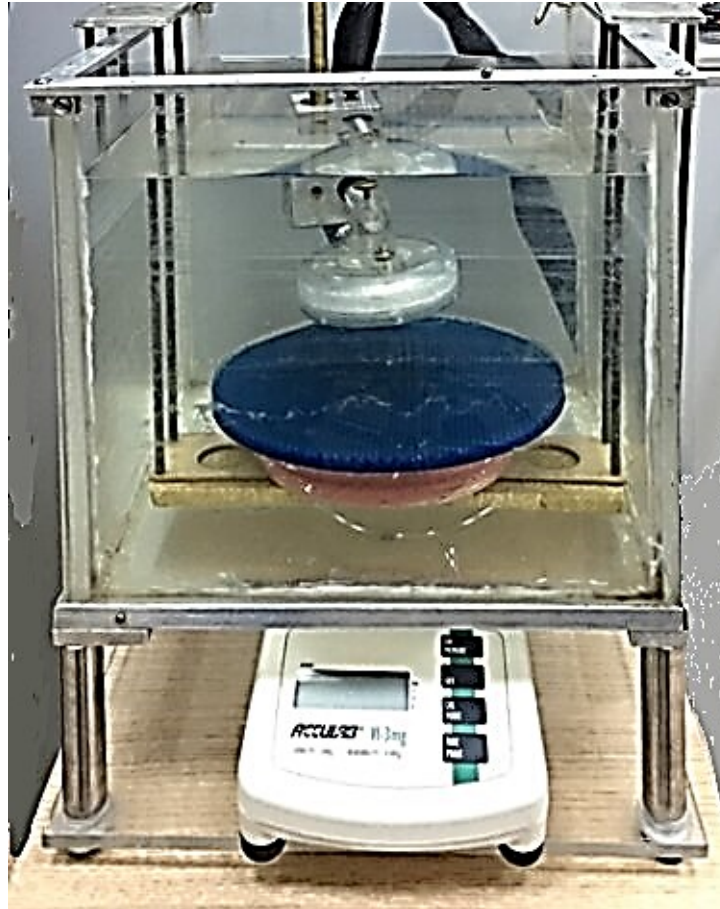
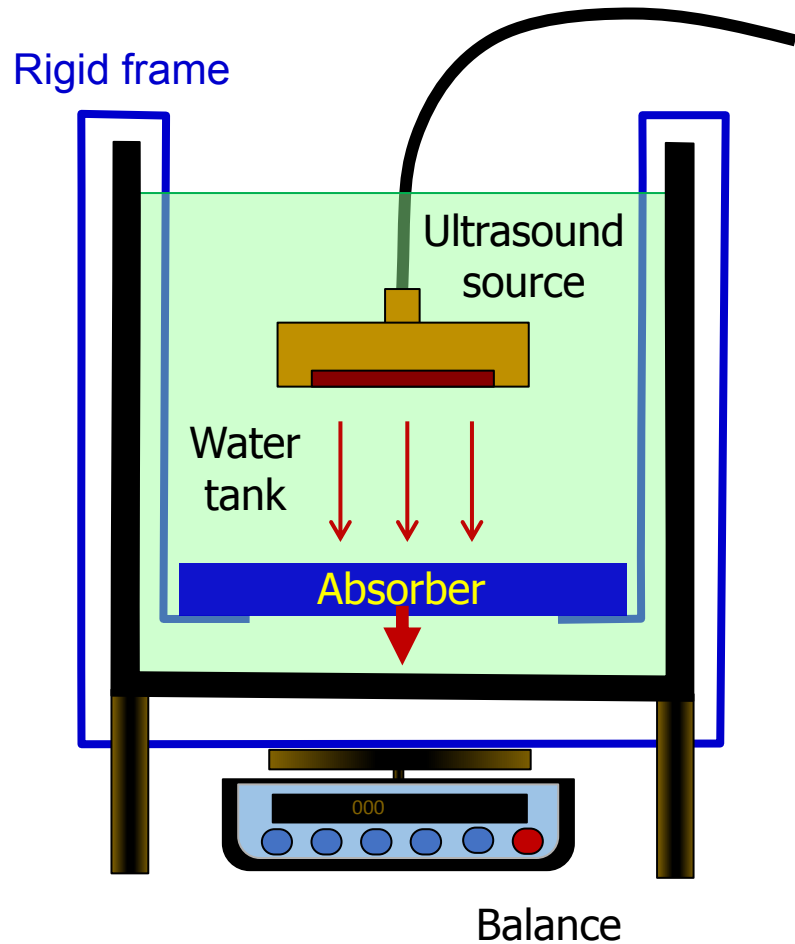
$$\Delta N / \Delta t = \frac{\Delta E / \Delta t}{c} \Rightarrow F = \frac{W}{c}$$

RADIATION FORCE ACTING ON AN EXTENDED ABSORBER



Change of weight / Acoustic power
68 mg / watt , i.e., 15 watt \leftrightarrow 1 g

RADIATION FORCE BALANCE



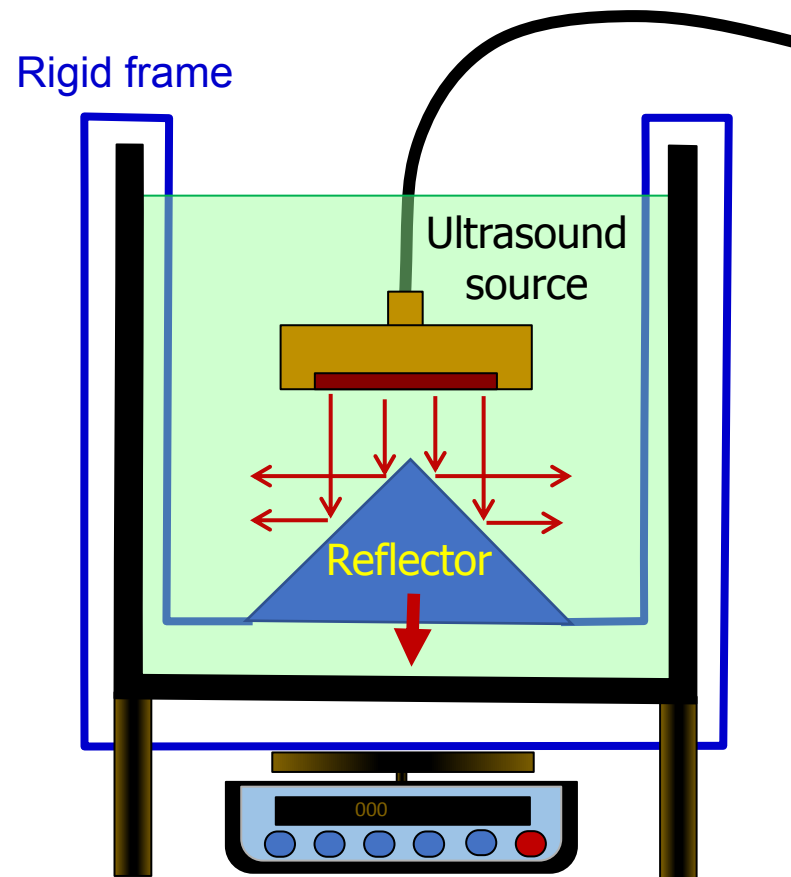
Measuring transducer power
2 weeks ago, in Seattle ...



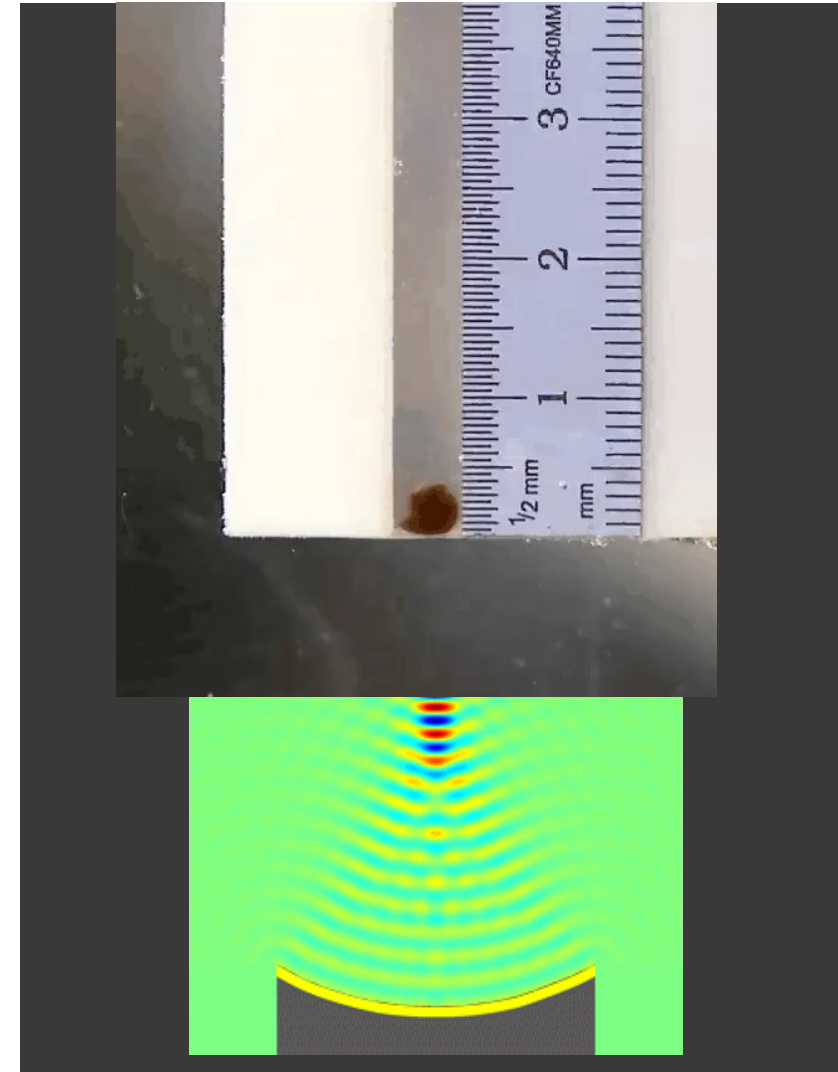
IEC STANDARD: IEC61161:2006, Ed.2. Ultrasonics – Power measurement – Radiation force balances and performance requirements, International Electrotechnical Commission, Geneva, 2006.

RADIATION FORCE ACTING ON A REFLECTOR (SCATTERER)

Radiation force balance
with conical reflector



Repulsion of kidney stones



Radiation force of an arbitrary acoustic beam on an elastic sphere in a fluid

$$S(k_x, k_y) = \int_{-\infty-\infty}^{+\infty+\infty} dx dy p_{inc}(x, y, 0) e^{-ik_x x - ik_y y}$$

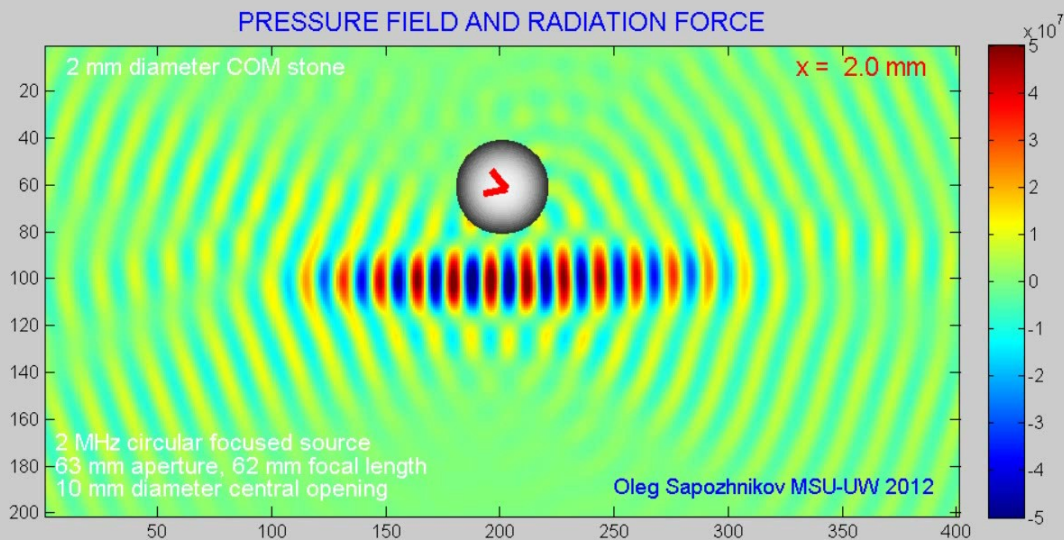
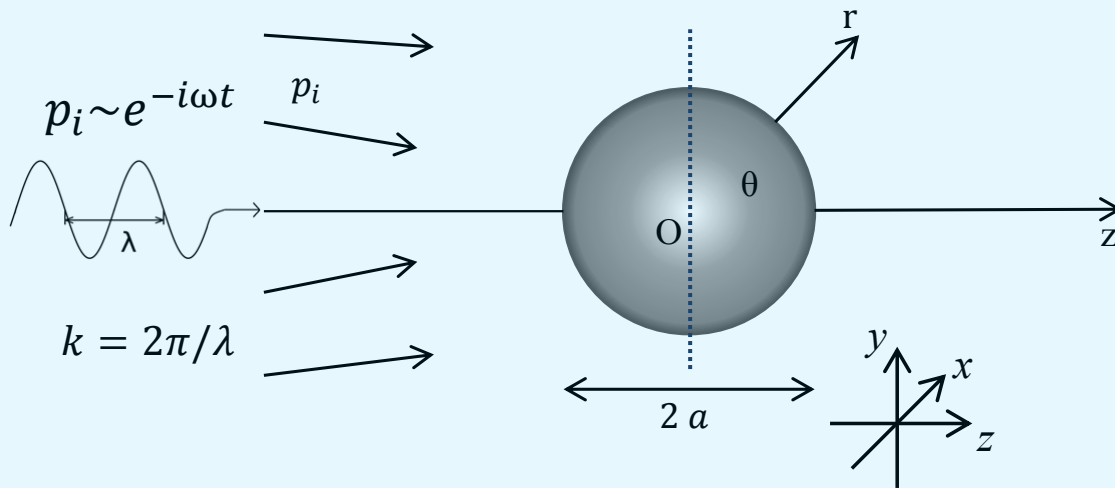
$$H_{nm} = \iint_{k_x^2 + k_y^2 < k^2} dk_x dk_y S(k_x, k_y) Y_{nm}^*(\theta_k, \phi_k)$$

$$F_z = -\frac{1}{4\pi^2 \rho c^2 k^2} \operatorname{Re} \left\{ \sum_{n=0}^{\infty} \Psi_n \sum_{m=-n}^n B_{nm} H_{nm} H_{n+1,m}^* \right\}$$

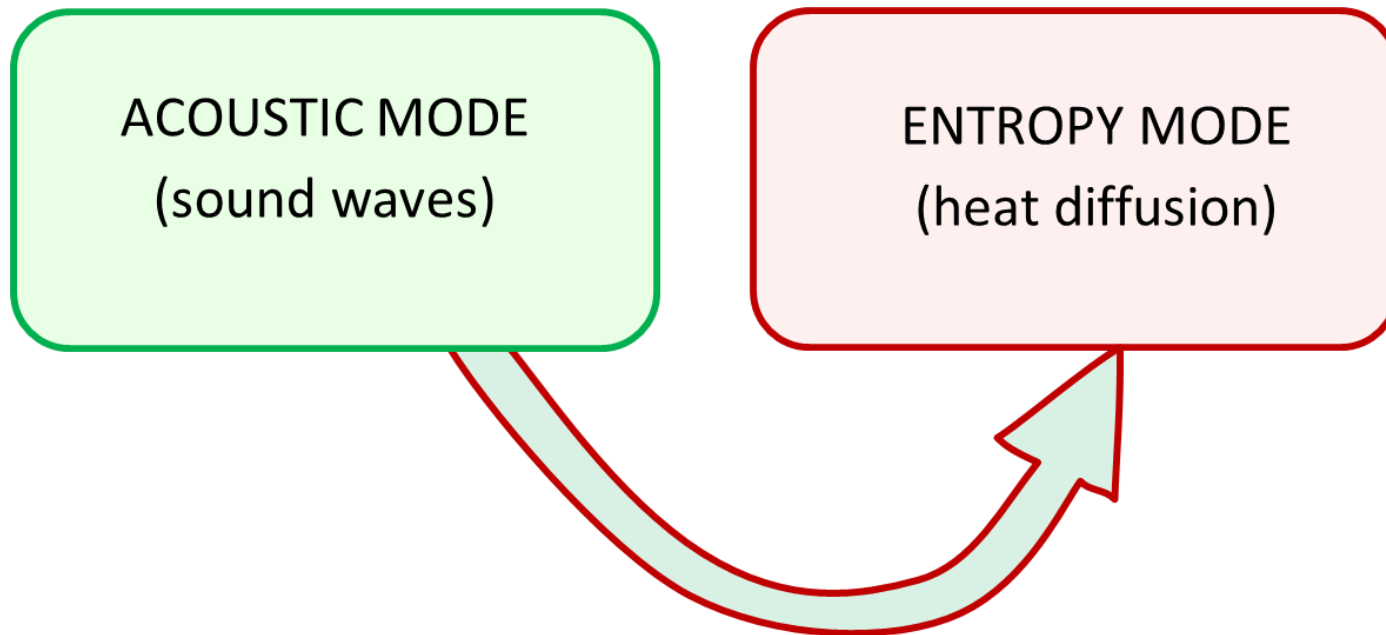
$$\Psi_n = (1 + 2c_n)(1 + 2c_{n+1}^*) - 1$$

$$B_{nm} = \sqrt{\frac{(n+m+1)(n-m+1)}{(2n+1)(2n+3)}}$$

Sapozhnikov, Bailey, JASA 2013



Excitation of the entropy mode by sound
(transfer of energy from sound to medium –
heating by acoustic waves)



Equations for classical thermoviscous fluid

$$\rho \left[\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} \right] = -\nabla p + \eta \Delta \mathbf{v} + \left(\zeta + \frac{\eta}{3} \right) \nabla (\nabla \cdot \mathbf{v})$$

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

$$\rho T \left[\frac{\partial s}{\partial t} + (\mathbf{v} \cdot \nabla) s \right] = \kappa \Delta T + \frac{\eta}{2} \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \nabla \cdot \mathbf{v} \right)^2 + \zeta (\nabla \cdot \mathbf{v})^2$$

Thermodynamic relations

$$d\rho = dp/c^2 - ds \cdot \alpha_V T \rho / c_p$$

$$dT = dp \cdot \alpha_V T / (\rho c_p) + ds \cdot T / c_p$$

Fluid parameters

$$\alpha_V = -\rho^{-1} (\partial \rho / \partial T)_p$$

$$c = \sqrt{(\partial p / \partial \rho)_s} \quad c_p = T (\partial s / \partial T)_p$$

BASIC EQUATIONS FOR THE HEAT PRODUCTION

Second law of thermodynamics $\delta Q = TdS$ corresponds to the following entropy balance equation:

$$\frac{\partial(\rho s)}{\partial t} + \nabla \cdot \mathbf{S} = \frac{1}{T} \frac{\partial Q}{\partial t}$$

$\mathbf{S} = \rho s \mathbf{v} + \frac{\mathbf{q}}{T}$ is entropy flux, where $\mathbf{q} = -\kappa \nabla T$ is Fourier's law. Equations of fluid dynamics provide the following amount of heat produced in the fluid per unit volume and time:

$$\frac{\partial Q}{\partial t} = \frac{\kappa}{T} (\nabla T)^2 + \frac{\eta}{2} \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \nabla \cdot \mathbf{v} \right)^2 + \zeta (\nabla \cdot \mathbf{v})^2$$

For a plane wave the energy dissipation (averaged over the wave period) per unit volume and time is

$$\left\langle \frac{\partial Q}{\partial t} \right\rangle_{\text{plane wave}} = \frac{\delta}{\rho_0 c_0^4} \left\langle \left(\frac{\partial p'}{\partial t} \right)^2 \right\rangle$$

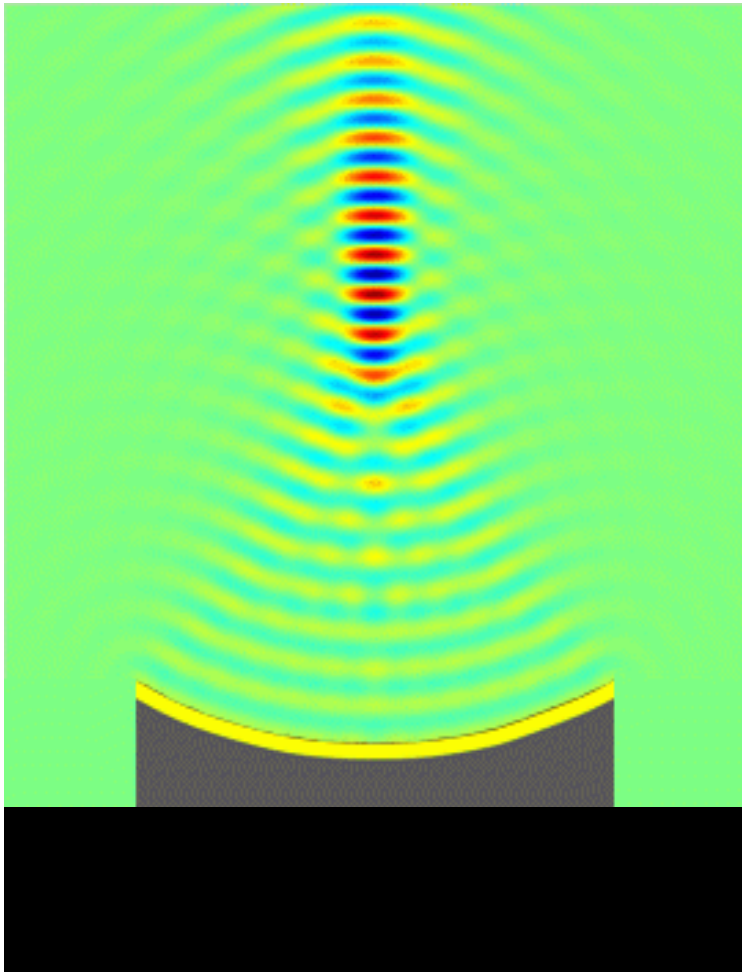
Here $\delta = [4\eta/3 + \zeta + \kappa(c_v^{-1} - c_p^{-1})]/\rho_0$ is the diffusivity coefficient. For a particular case of a propagating harmonic wave $I = \langle p'^2 \rangle / (\rho_0 c_0)$ is wave intensity, which gives

$$\left\langle \frac{\partial Q}{\partial t} \right\rangle_{\text{plane sine wave}} = 2\alpha I$$

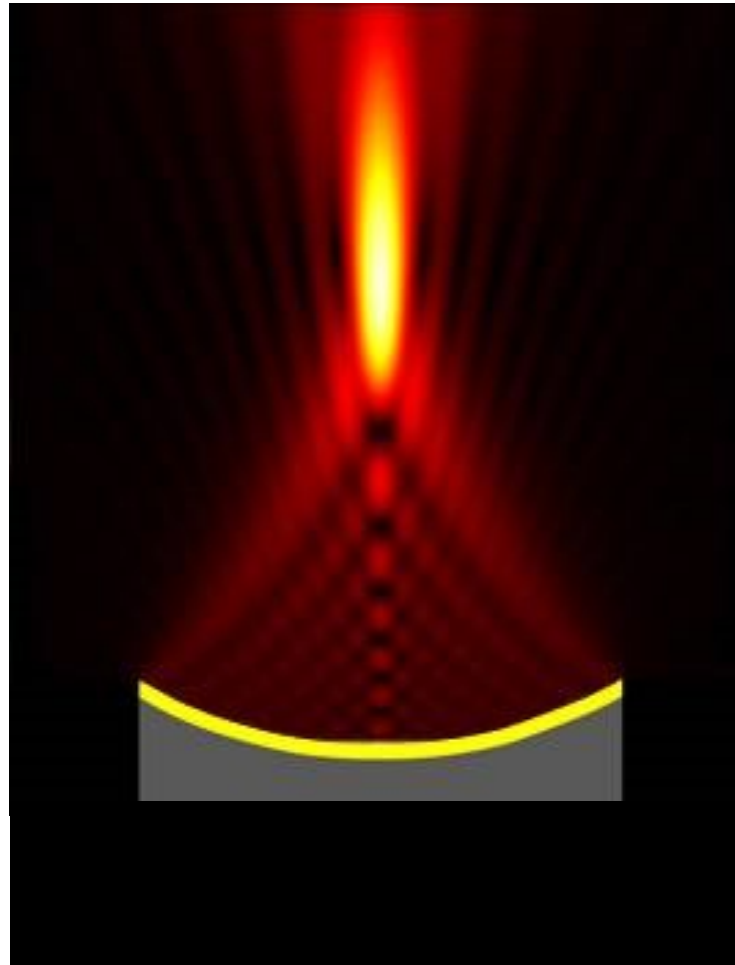
Acoustic field of a focused ultrasound source and associated heating

$$\left\langle \frac{\partial Q}{\partial t} \right\rangle_{\text{plane sine wave}} = 2\alpha I$$

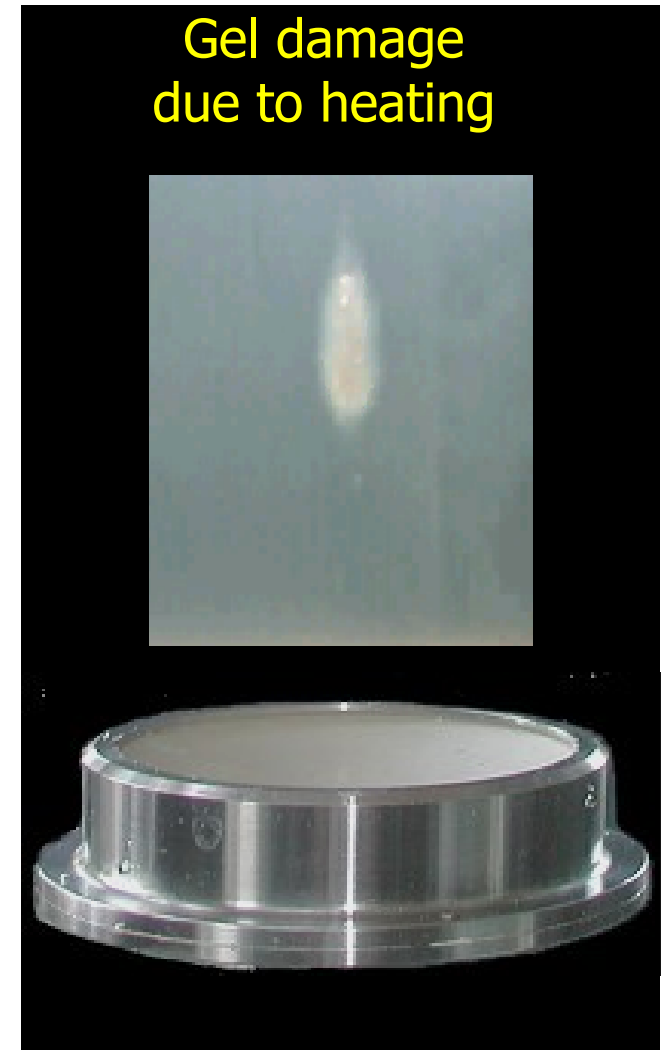
Acoustic pressure, p'



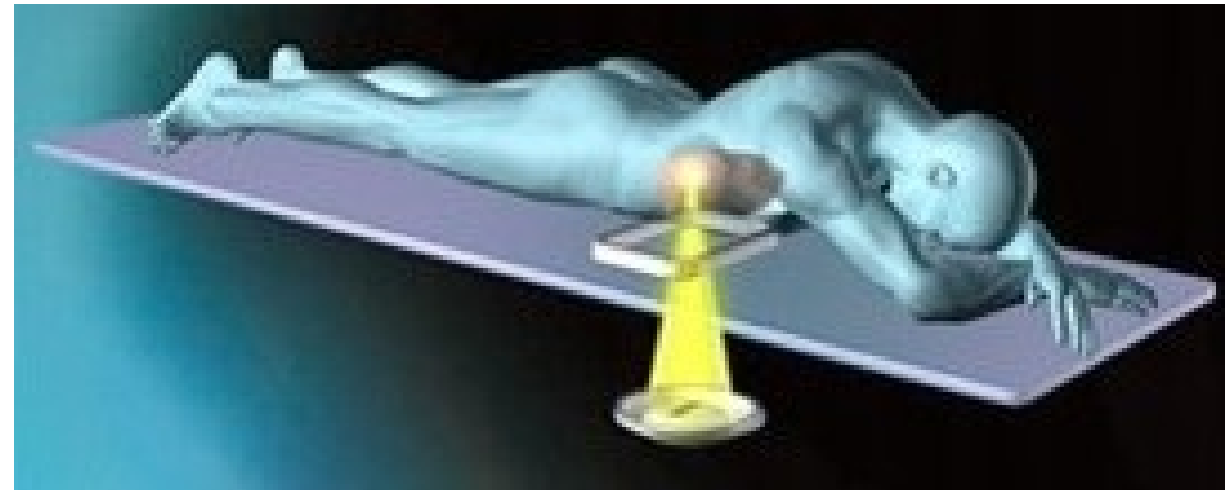
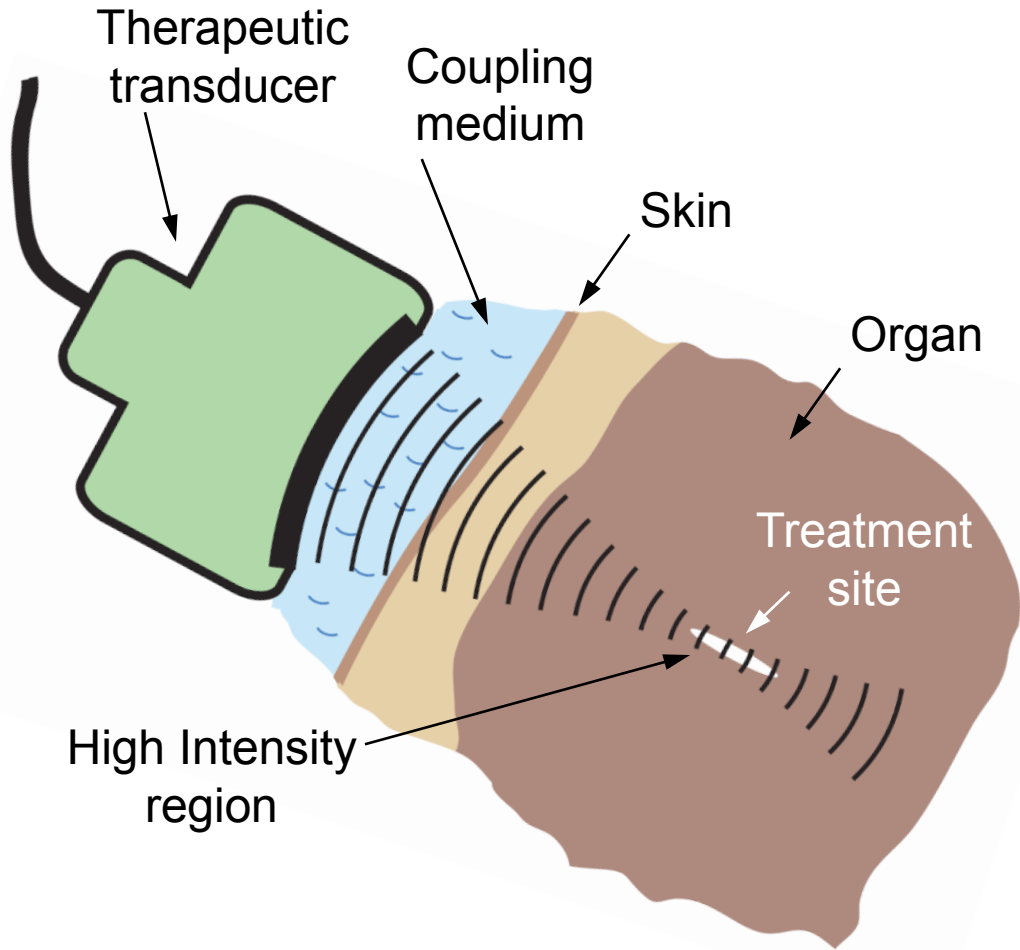
Intensity, $I = \langle p'^2 \rangle / (\rho_0 c_0)$



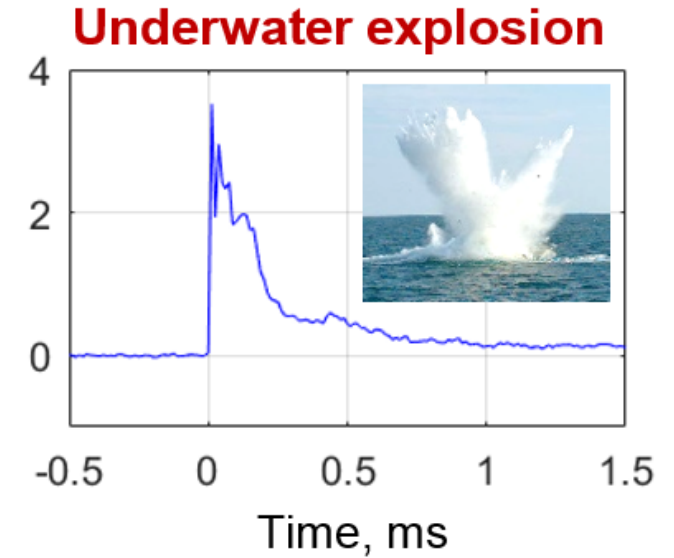
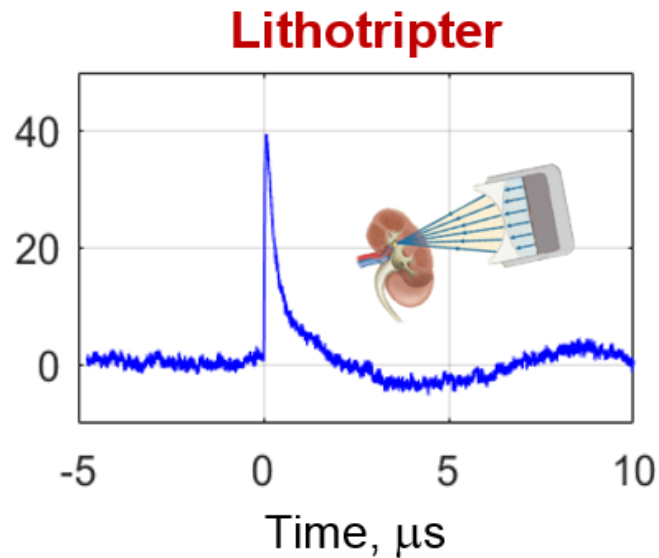
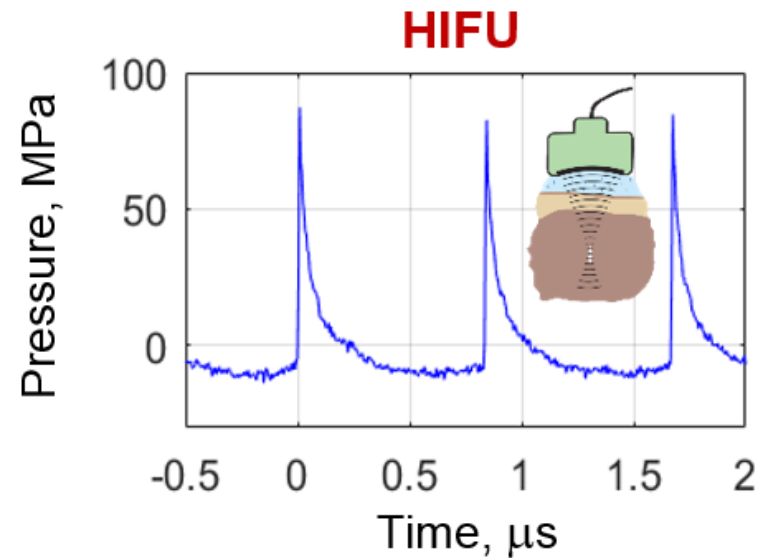
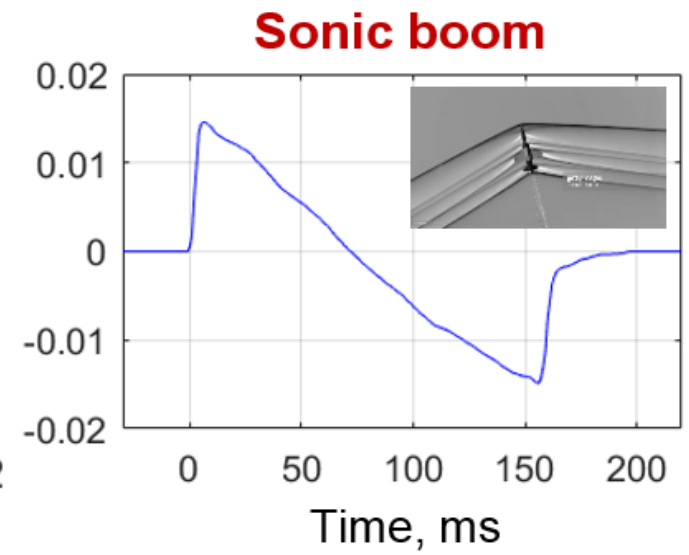
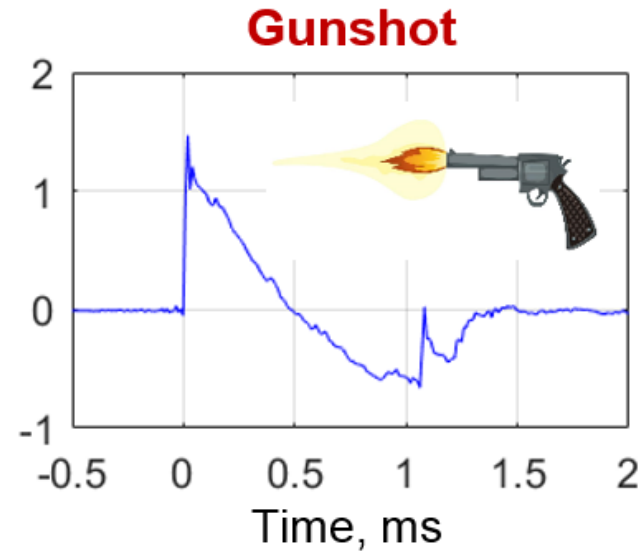
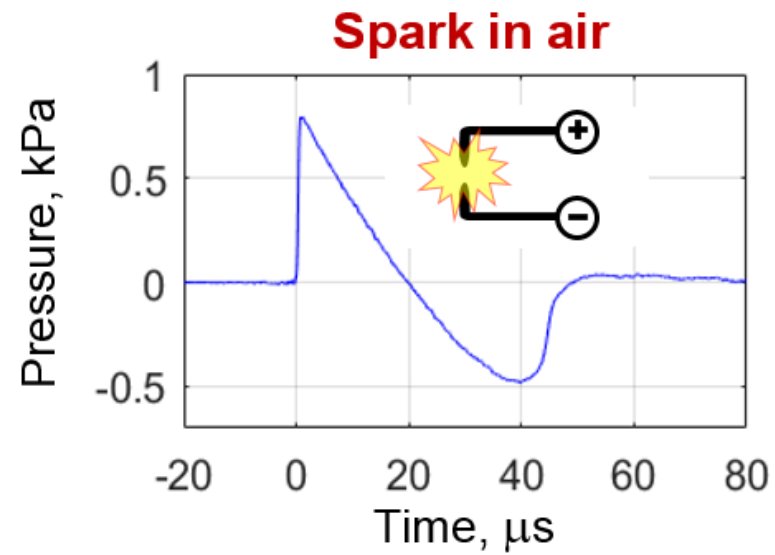
Gel damage
due to heating



Use of high-intensity focused ultrasound (HIFU) for therapy and surgery



Weak shock waves resulting from nonlinear propagation



Entropy (and therefore, heat) production at the shock front

$$\Delta s = \frac{\beta}{6\rho_0^3 c_0^4 T_0} (\Delta p)^3$$

$$Q_{\text{shock}} = \rho_0 T_0 \Delta s = \frac{\beta}{6\rho_0^2 c_0^4} (\Delta p)^3$$

$$\left\langle \frac{\partial Q}{\partial t} \right\rangle_{\text{sawtooth wave}} = \frac{\beta f_0}{6\rho_0^2 c_0^4} (\Delta p)^3$$

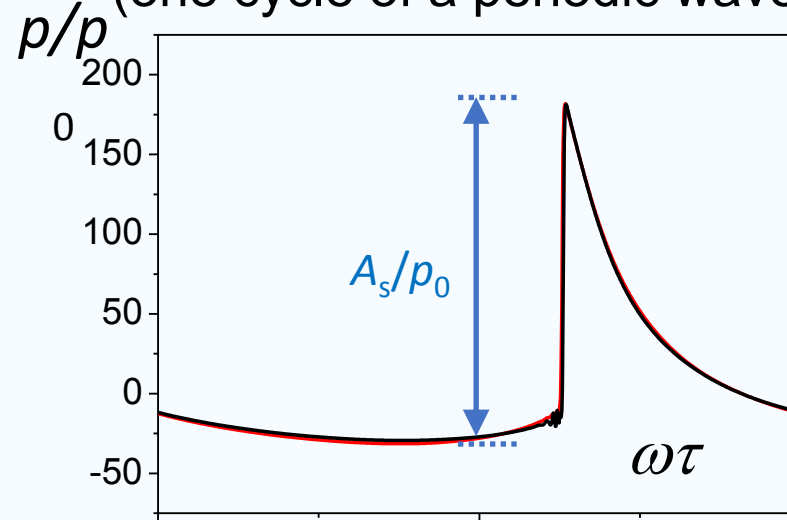
$$\left\langle \frac{\partial Q}{\partial t} \right\rangle_{\text{plane sine wave}} = 2\alpha I = \alpha \frac{A_0^2}{\rho_0 c_0}$$

$$\frac{\left\langle \partial Q / \partial t \right\rangle_{\text{sawtooth wave}}}{\left\langle \partial Q / \partial t \right\rangle_{\text{sine wave}}} = \frac{2}{3} \frac{\beta f_0}{\alpha \rho_0 c_0^3} \Delta p \gg 1 \text{ for large } \Delta p$$

Fast boiling at the HIFU focus in shockwave regime

Canney *et. al.* UMB, v.36 (2010)

Focal waveforms in water
(one cycle of a periodic wave)

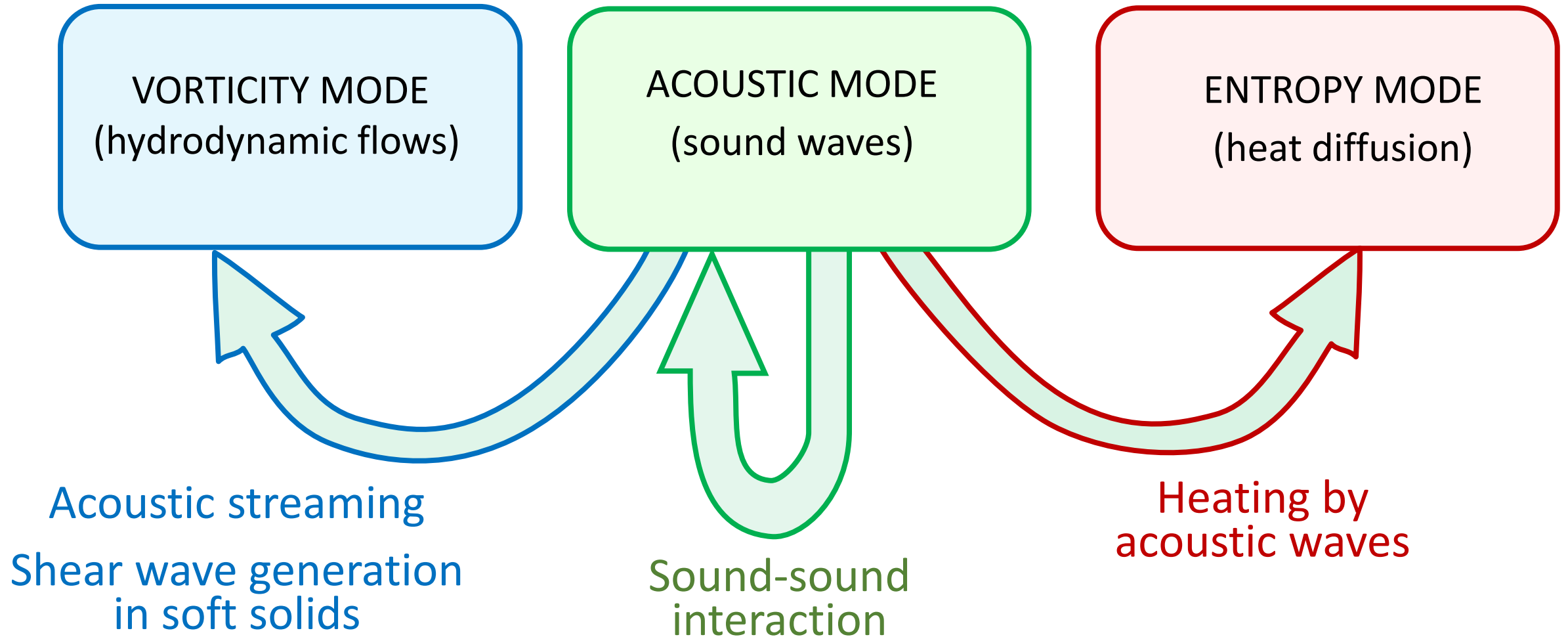


Gel near the focus



Tissue at the focus can reach
100°C in a millisecond!

THE SUBJECTS OF STUDY IN NONLINEAR ACOUSTICS



SHORT COURSE ON NONLINEAR ACOUSTICS - to be continued



David Blackstock (1930–2021) in Seattle, 2020

WHAT TO READ

1. Hamilton, M.F., and Blackstock, D.T. (Eds.). *Nonlinear Acoustics*. – Acoustical Society of America, Melville, NY, 2008.
2. Rudenko, O.V., and Soluyan, S.I. *Theoretical Foundations of Nonlinear Acoustics*. – Consultants Bureau, London, 1977.
3. Naugolnykh, K., and Ostrovsky, L. *Nonlinear Wave Processes in Acoustics*. – Cambridge Univ. Press, Cambridge, 1998.
4. Pierce, A.D. *Acoustics: An Introduction to Its Physical Principles and Applications*. – Acoust. Soc. Am., 1994.
5. Landau, L.D., and Lifshits, E.M. *Fluid Mechanics*. – 2nd ed., Pergamon, New York, 1987.
6. Chu, B.-T., and Kovasznay, L.S.G. Non-linear interactions in a viscous heat-conducting compressible gas. – *Journal of Fluid Mechanics* **3**, 494–514 (1958).
7. Pierce, A.D. Entropy, acoustic, and vorticity mode decomposition as an initial step in nonlinear acoustics formulations. - *Nonlinear Acoustics at the Beginning of the 21st Century*, edited by O.V. Rudenko and O.A. Sapozhnikov (Faculty of Physics, MSU, Moscow, 2002), vol. 1, pp. 11–19.
8. Nyborg, W.L. Acoustic streaming, in *Physical Acoustics* (W. P. Mason, ed.), vol. 2, Pt B, ch. 11, 265–331, New York, NY: Academic Press, 1965.
9. Lighthill, J. Acoustic streaming. *J. Sound Vib.* **61**, 391–418 (1978).
10. McIntyre, M.E. On the ‘wave momentum’ myth. – *J. Fluid Mech.* **106**, 331–347 (1981).
11. Sapozhnikov, O.A., and Bailey, M.R. Radiation force of an arbitrary acoustic beam on an elastic sphere in a fluid. – *J. Acoust. Soc. Am.* **133**(2), 661–676 (2013).
12. Sapozhnikov, O.A. High-intensity ultrasonic waves in fluids: Nonlinear propagation and effects. - In: *Power Ultrasonics. Applications of High-intensity Ultrasound*, ed. by Gallego-Juarez, J.A., and Graff, K.F., Chapter II, Woodhead Publishing Series in Electronic and Optical Materials (Elsevier), Cambridge, №66, pp. 9–35 (2014).